

OPTIMIZATION OF EDTA ENHANCED SOIL WASHING ON MULTIPLE HEAVY METALS REMOVAL USING RESPONSE SURFACE METHODOLOGY

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Abstract. This research presents the optimization of soil washing conditions in the removal of multiple heavy metals (Cu-Pb-Zn-Cd) under the using of ethylenediaminetetraacetic acid (EDTA). The optimum combination of washing parameters in a bench-scale soil washing experiments is determined by response surface methodology (RSM). Central composite design is applied after single factor experiment, EDTA concentration, solid-to-liquid ratio and washing time are evaluated variables for the removal processes, and the regression models of HMs are constructed. The results show that, EDTA concentration and solid-to-liquid ratio are significant factors for this process. Subsequently, 50% of Cu removal was set as the optimum target to optimize the combined conditions, through the building of multiple quadratic regression models, the optimal condition combination is determined that EDTA concentration is $0.0026 \text{ mol}\cdot\text{L}^{-1}$, solid-to-liquid ratio is 1:22, washing time is 3.89 h, the extraction rate of Pb, Zn, Cd is predicted to be 78%, 75% and 71%, respectively.

Keywords: soil cleaning technologies, soil washing, multiple heavy metals pollution, response surface methodology.

Introduction

Soil pollution caused by heavy metals (HMs) has become a widespread global problem for their non-biodegradation and long residence time (Wuana, Okieimen, & Imborvungu, 2010; Evangelou, Bauer, Ebel, & Schaeffer, 2007). HMs pollutants in the soil could lead to adverse effects on environment and serious threat to humans (Ferraro, Fabbicino, Hullebusch, Esposito, & Pirozzi, 2016). Single type of heavy metal has been intensively studied of late years, nevertheless, a number of HMs always co-exist in common types of contamination sites (Arao et al., 2010; Moutsatsou, Gregou, Matsas, & Protonotarios, 2006). In many parts of the world, soil HMs derives normally from long-term utilization of phosphatic fertilizers, mining and smelt industry, and sewage sludge disposal (Ciccu et al., 2003; Xia et al., 2009; Mandal, Purakayastha, & Patra, 2014). Multiple Multiple HMs pollution of soils is one of the environmental concerns in recent decades, which led to consequently urgent need of effective remediation technologies.

Various techniques for the removal of HMs from contaminated soils, have been investigated and adopted to reduce the prospective healthy and migration risk. For instance, solidification/stabilization, soil flushing,

phytoremediation, microbial remediation and soil washing (Wasay, Barrington, & Tokunaga, 2013; Dermont, Bergeron, Mercier, & Richerlaflèche, 2008), among them, ex-situ soil washing has becoming a more and more widely used method due to its simple operation, efficiency, and barely limited by site environment (Daniel, Irene 2006; Tsang & Lo, 2006; Voglar & Lestan, 2012). Ex-situ soil washing process bases on the idea of water rinsing to remove pollutants from soil and to transfer them to a concentrated liquid phase (Mao, Jiang, Xiao, & Yu, 2015). Generally speaking, it includes either a physical separation, or a chemical extraction, although both the physical and the chemical washing often coexist in most cases (Peters, 1999; Di Palma, Ferrantelli, & Medici, 2005). Many different chemicals like acid solutions, diluted acid solutions containing chloride salts, surfactants, reducing and oxidizing agents, and chelants are of high extraction efficiency for HMs in the soil (Dermont et al., 2008). For the purpose of removing various types of contaminant from soil, chemical-enhanced soil washing has been comprehensively studied in recent years (Lo, Tanboonchuy, Yan, Grisdanurak, & Liao, 2012; Gao, He, Ling, Hu, & Liu, 2003; Haapea & Tuhkanen, 2006).

A variety of factors contribute to the effectiveness of the washing process, including properties of the target

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contaminants, soil texture and extraction solution, among them, the type of washing solution is of critical importance (Mulligan, Yong, & Gibbs, 2001). Chelating agents are always used to improve remove ability in physical-chemical remediation. Among them, ethylenediaminetetraacetic acid (EDTA) has strong chelating ability for different heavy metals (Sun, Zhao, & Lombi, 2001; Leštan, Luo, & Li, 2008; Finzgar, Jez, Voglar, & Lestan, 2014; Guo et al., 2016), which is cited frequently as an effective agent in the removal of HMs from contaminated soils, thus, EDTA was chosen as the washing solution in this study.

The majority of reported studies of optimization of chemical process parameters involved with the method of changing one variable while maintaining other formulation variables constant, which was not only time-consuming and tedious, but also giving rise to the cost (Lo et al., 2012). Comparatively speaking, design of experiments (DoE) approach has become a useful tool in quality controlling for both single-factor and multi-factor experiment (Lionberger, S. L. Lee, L. Lee, Raw, & Yu, 2008). Takes full use of DoE in predictive model construction of the critical response variables could facilitate identification of all potential independent variables and their simultaneous systematic and rapid evaluation (Poudel et al., 2012). Response surface methodology (RSM) is a collection of statistical and mathematical DoE techniques for modeling and analysis responses influenced by several variables, which are more reliable than unplanned experiments (Dean & Voss, 2010). Numerous studies have described RSM in metabolites producing from microorganisms (El-naggar, Elshweihy, & Elewasy, 2016; Hwang et al., 2012), culture conditions determination in extracellular metabolites producing (Shen et al., 2014; Moradpour, Ghasemian, Mohkam, & Ghasemi, 2012), and drug producing (Gupta et al., 2016), whereas, it was rarely used in optimization of chemical processes. Therefore, the purpose of this study was using central composite design (CCD) of RSM to optimize the conditions for the removal of Cu, Pb, Zn and Cd from the contaminated soils in the process of soil washing with EDTA. The relationship between the response (remove rate) and input variables (EDTA concentration, washing time, solid-to-liquid ratio) were fit and explored. A batch of experiments was designed, and the removal effect was determined by the remove rate of the total concentration of HMs in the soil.

1. Materials and methods

1.1. Soil sampling and preparation

Surface soils (0–20 cm) were collected from 5 sample points in paddy field in southwest of China. Soil samples were blended well after taking to the laboratory, then air-dried under room temperature. Coarse debris and visible plant materials were eliminated by a 1mm nylon sieve. The soil pH was measured in a 1:2.5 (w/v) ratio of soil and 0.01M CaCl₂ water solution suspensions. The soil organic matter was determined by potassium bichromate

titrimetric method described in GB 9834-88:1988. *Method for determination of soil organic matter*. The cation exchange capacity was analyzed using the ammonium acetate method, and the soil particle distribution was measured by laser granulometry (Beckman Coulter, LS230). The physicochemical properties of soil show that soil pH value was 6.5, organic matter was 20.3 g·kg⁻¹, cation exchange capacity was 17.5 cmol·kg⁻¹, moisture content was 6.4%, sand percentage is 10.3%, clay percentage is 21.4%, silt percentage is 38.3%.

Total metal concentrations in paddy field were: Cu 122 mg·kg⁻¹, Zn 195 mg·kg⁻¹, Pb 41 mg·kg⁻¹, Cd 0.01 mg·kg⁻¹, suggesting that only Cu pollution existed in the applied soil according to the Chinese National Standard of the Environmental quality standard for soils (GB 15618-1995), pH below 6.5 for paddy soil, the standard value is Cu 50 mg·kg⁻¹, Zn 200 mg·kg⁻¹, Pb 250 mg·kg⁻¹, Cd 0.30 mg·kg⁻¹, respectively.

Since sampling of natural severely polluted agricultural soil with multiple heavy metals is difficult, spiked soil by artificially contamination with heavy metal solution were frequently adopted in the lab (Kulikowska, Gusi-atin, Bułkowska, & Kierklo, 2015; Kang & So, 2016; Cameselle & Pena, 2016). In order to meet the study objective of exploring the removal efficiency of EDTA enhanced soil washing in multiple heavy metals contaminated soil, Cd(NO₃)₂, Cu(NO₃)₂, Zn(NO₃)₂, Pb(NO₃)₂ solutions were added to the pretreated soil samples to simulate contaminated soils. Spiked soil samples were left at room temperature for one month, and distilled water were added at regular intervals to keep field capacity at about 10% level.

For the purpose of keeping the soil pH at the value of 6.0, HCl solution of 0.01mol·L⁻¹ was used to adjust pH value from 6.5 to 6.0, NaOH solution of 0.01mol·L⁻¹ was used to neutralize the excessive amount of HCl during the experimental operation. Afterwards, simulated soil samples were kept at room temperature then naturally air-dried. Total metal concentrations in artificially contaminated soils were: Cu 668 mg·kg⁻¹, Zn 383 mg·kg⁻¹, Pb 397 mg·kg⁻¹, Cd 31 mg·kg⁻¹.

1.2. Chemical agents

EDTA solutions of 0.001, 0.002, 0.003, 0.005, 0.010 and 0.015 mol·L⁻¹ were prepared with 0.01 mol·L⁻¹ NaNO₃ solution to control ionic strength, 0.01mol·L⁻¹HCl and 0.01 mol·L⁻¹ NaOH solution were used to adjust pH. Chemical agents used in the experiment were of analytical grade purity.

1.3. Statistical analysis

RSM is divided into two categories, Box-Behnken design (BBD) and CCD. The latter approach was selected to evaluate the interaction of different factors and their effects on EDTA washing. CCD requires less number of experiments, which is a valuable tool to assess the optimization responses shaped under the influence of multiple

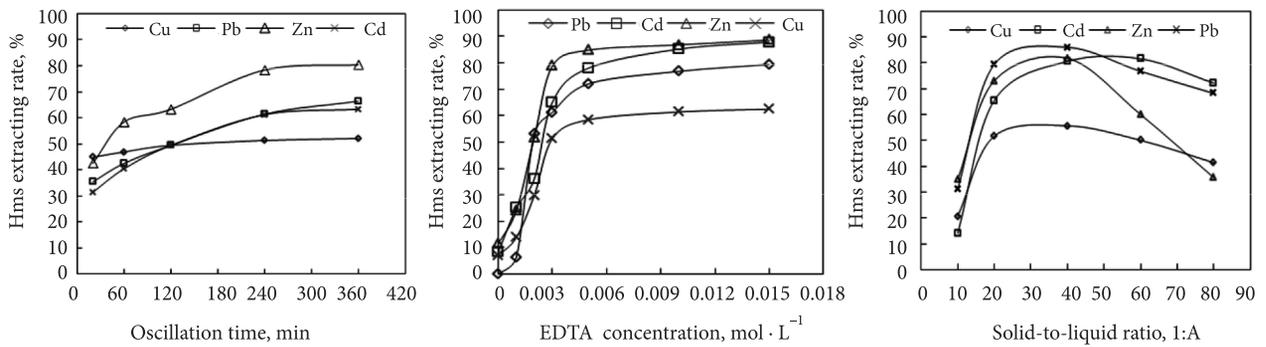


Figure 1. Effect of single process parameter on EDTA enhanced soil washing

independent factors and their degree of interaction (Tanyildizi, 2011; Sugashini & Begum, 2013). It could probe the optimum level of each factor by building a mathematical model and generating three-dimensional (3D) response surface images, which could give better prediction and directly overview for the parameter optimization (Madeira, Ribeiro, Turk, & Cabral, 2010).

The one-variable-at-a-time method was used as the first step to determine the equilibrium values, which were chosen as center points used in the next step of experimental design. Basing on synthesized analysis of four types of HMs in this work, highest extracting rate was set as the optimization target, CCD experiments were implied to obtain their optimum combination.

In our study, the responses, which were the dependent variables, were the extraction rates of Cu (Y_1), Pb (Y_2), Zn (Y_3) and Cd (Y_4). EDTA concentration (A), solid-to-liquid ratio (B), and oscillating time (C) were selected as independent variables. The CCD experiments of three variables, each had 5 levels (± 1 for the factorial points, 0 for the center point, and $\pm \alpha$ for the axial points), which has allowed estimation of a full quadratic model with the general description: $N = 2^k - p + 2k + C_0$, where N is the number of experiments, k is the number of independent variables ($k = 3$), p the fractionalization number (in a full design, $p = 0$) and C_0 is the number of central points ($C_0 = 6$), required for curvature estimation (Barker, 1985).

The design and result analysis of CCD experiment were performed by using Design Expert 8.0.6.1 (Stat-Ease, Inc Minneapolis, MNUSA). The lowest and the highest levels of variables were given in Table 1.

2. Results and discussion

2.1. Results of EDTA washing experiment

The washing processes were carried out with 1.0 g soil samples mixed with EDTA solution in 50 mL centrifuge tubes, the suspensions were oscillated at 20 °C with pH value fixed at 6. After oscillating, the samples were centrifuged at 4000 r/min for 10 min and filtered by 0.45 μ m micropore filter, supernatants were separated to measure metal concentrations by inductively coupled plasma

Table 1. Uncoded and coded levels of the independent variables

Independent variables		Coded levels				
		-2	-1	0	1	2
A	EDTA concentration /mol·mL ⁻¹	0	0.001	0.003	0.005	0.006
B	Solid-to-liquid ratio	1:5	1:10	1:20	1:30	1:35
C	Washing time/h	1	2	4	6	7

mass spectroscopy with experiment detection limits at 0.01 mg·L⁻¹.

Washing time, EDTA concentration, and solid-to-liquid ratio were probed to assess their effects on EDTA enhanced soil washing. Batches of experiments were conducted to optimize the value for each parameter for further experiments. The time used in oscillation was set from 10 min to 480 mins (10, 20, 40, 60, 120, 240, 360, 480 mins) with 50 mL 3 mmol·L⁻¹ EDTA solution added to 1g soil samples to optimize the washing time. The effect of EDTA concentration was studied by adding 50 mL 0.001 mol·L⁻¹ to 0.015 mol·L⁻¹ EDTA solutions (0.001, 0.002, 0.003, 0.005, 0.01, 0.015 mol·L⁻¹) in soil samples with 4 hours oscillation. Solid-to-liquid ratio, ranged from 1:20 to 1:80 (w/v) with an interval of 20, was studied by adding 20, 40, 60 and 80 mL 0.003 mol·L⁻¹ EDTA solution to 1g soil sample with 4hours oscillation, respectively. All of the washing disposes were triplicated, and the average of extracting rate was taken as the dependent variable or response.

The results showed that extraction rates of four varieties of HMs, Cu, Pb, Zn, Cd were basically of consistent tendency under selected variables. As the values of selected variables increased, the extraction rates inhibited a rapid improvement at first and then gradually remained constant and rose to an equilibrium (Figure 1).

2.2. Central Composite Design experimental results

A total of 20 ($2^3 - 0 + 2 \times 3 + 6$) combinations (including six replicates of the central point each signed the coded value 0) were chosen according to a CCD configuration

for three independent variables. The results of HMs extraction rate were showed in Table 2.

2.3. Development of regression model

Regression models were built, and the analysis of variance (ANOVA) were conducted.

(a) Regression model analysis of extraction rate of Cu.

The second-order polynomial regression equation showing the relationship between the Cu extraction rate and three test variables is presented in Eq. (1):

$$Y_1 = -71.3301 + 25.30233 \times A + 5.48281 \times B + 1.43325 \times C - 0.24836 \times A \times C - 0.087287 \times A \times B + 0.010889 \times B \times C - 1.94315 \times A^2 - 0.084118 \times B^2 - 0.12339 \times C^2, \quad (1)$$

where Y_1 is the extraction rate of Cu; A is the concentration of EDTA solution ($10^{-3} \text{ mol}\cdot\text{L}^{-1}$); B is the ratio of solid-to-liquid; C is the time of oscillation.

The results of analysis of ANOVA for Y_1 were showed in Table 3. The model was statistically extremely significant at the 95% confidence level ($P < 0.0001$). Lack of fit test was determined by the ratio of lack of fit error to pure error (MS_{LF}/MS_{PE}). P value of lack of fit was not significant, which meant that there was no evidence of lack of fit. In general, the R^2 value was between 0 and 1, the closer the R^2 approximates to 1, the stronger is the model and the better it predicts the response (Gangadharan, Sivaramkrishnan, Nampoothiri, Sukumaran, & Pandey, 2008). The coefficient of determination (R^2) was calculated to be 0.9816, which means that the model explains

Table 3. ANOVA for the reduced quadratic model (Eq. 1)

Source	df	SS	MS	Prob > F
Model	9	841	120	<0.0001
A	1	3467	495	<0.0001
B	1	2508	358	<0.0001
C	1	8	1.15	0.308
AB	1	197	28	0.0003
AC	1	0.98	0.14	0.7169
BC	1	0.38	0.06	0.8207
A ²	1	623	89	<0.0001
B ²	1	729	104	<0.0001
C ²	1	2.51	0.36	0.5627
residual	10	7		

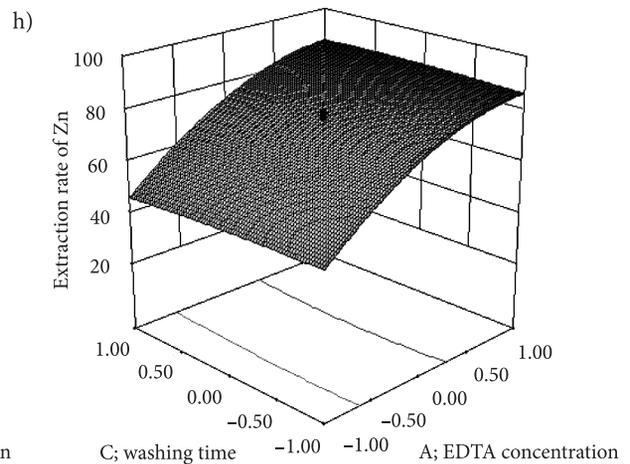
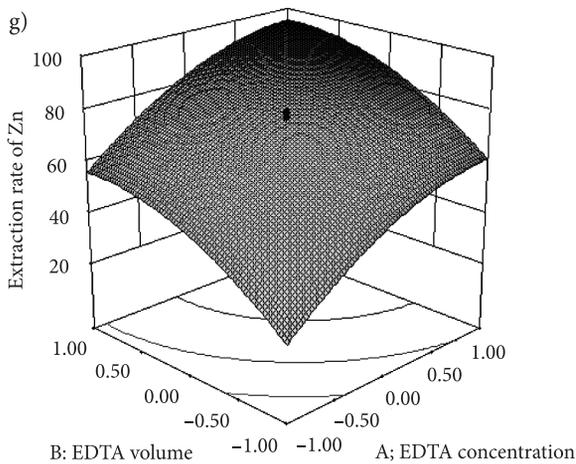
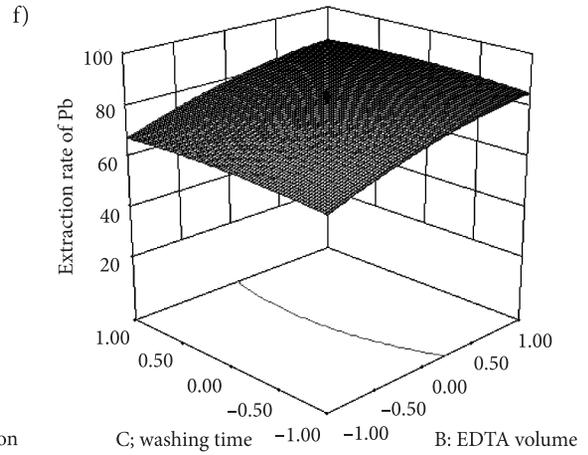
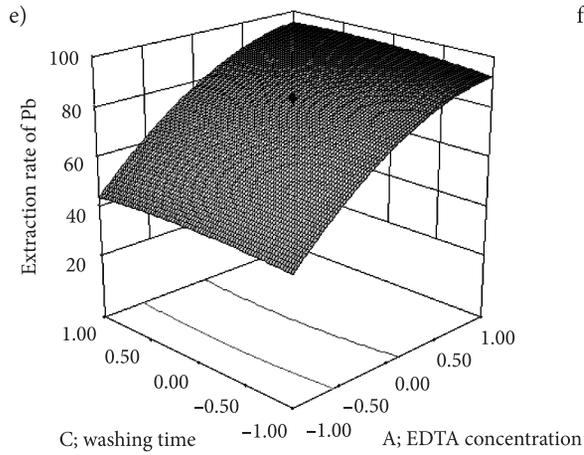
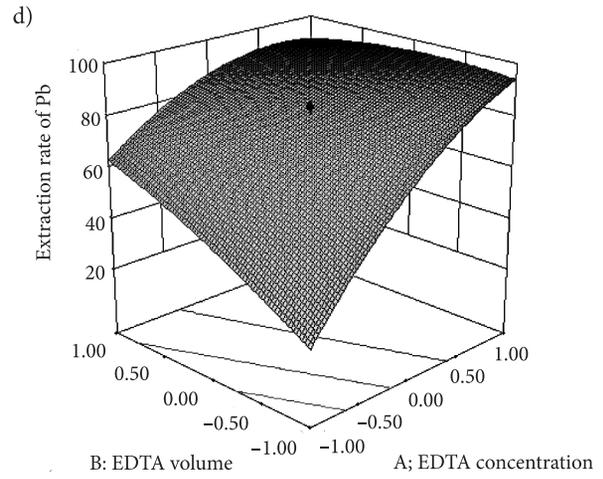
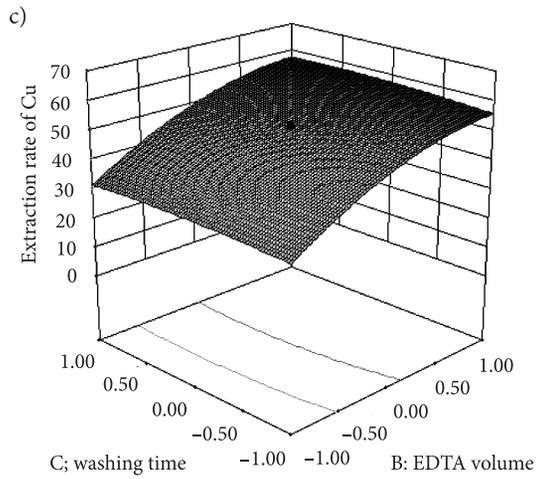
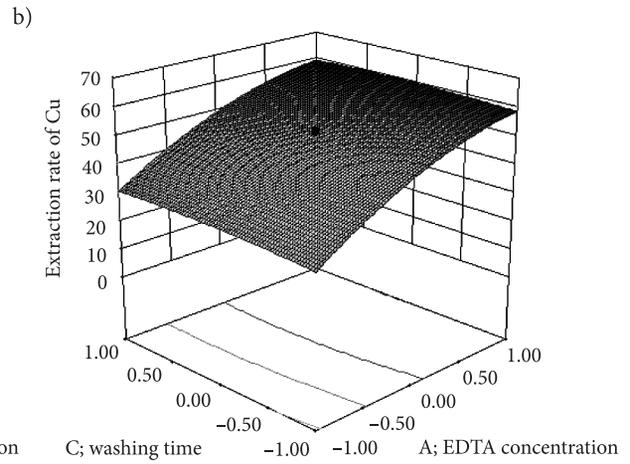
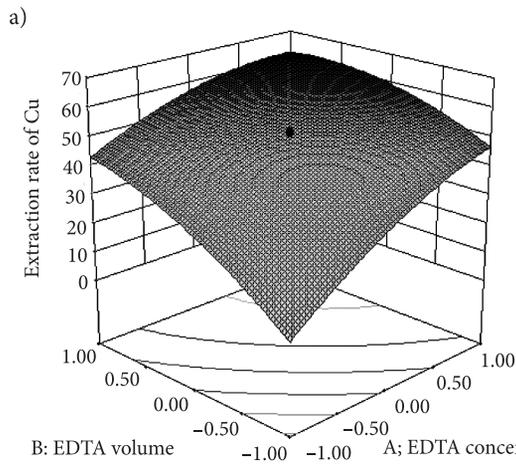
98.16% of the values in the experiment. The model for Y_1 was well fitted.

The relationships between independent and dependent variables can be easily visualized using RSM, where the obtained regression model was used to calculate the response surface for each response variable. The significance of the coefficients represented by P value is a valid parameter in checking the pattern of mutual interactions between variables (Khosravi, Vasheghani, Shojaosadati, & Yamini, 2004). For Y_1 , two main factors (A , B), one interaction term (AB), and two second order factors (A^2 , B^2) were significant ($P < 0.05$). It indicated that the extraction rate of Cu was significantly influenced by EDTA concentration and solid-to-liquid ratio, and there was an obvious interaction between EDTA concentration and solid-to-liquid ratio. The order of factors that affected the extraction

Table 2. Experimental design and results for CCD of response surface methodology

Code	A	B	C	Extraction rate/% (Y)							
				Y_1^a	Y_1^b	Y_2^a	Y_2^b	Y_3^a	Y_3^b	Y_4^a	Y_4^b
1	0	20	4	9.9	8.4	4.2	5.8	10.9	20.5	16.0	21.4
2	1	30	6	37.8	38.3	55.3	56.6	46.4	48.5	28.8	41.3
3	3	20	4	52.0	59.3	83.7	83.1	77.0	78.5	73.8	76.3
4	1	10	2	0.7	0.1	3.3	-6.3	17.8	13.8	6.5	9.0
5	1	10	6	0.9	0.5	4.3	-6.5	12.6	11.0	8.4	8.8
6	3	20	7	51.7	53.9	84.5	87.1	79.4	78.0	74.7	69.9
7	3	20	4	51.3	59.3	83.9	83.1	78.7	78.5	75.4	76.3
8	1	30	2	33.7	41.0	56.2	56.8	48.9	51.4	40.6	50.7
9	3	20	4	52.0	59.3	83.9	83.1	78.7	78.5	75.4	76.3
10	5	10	6	45.7	46.9	81.6	77.6	57.1	54.6	62.3	57.4
11	5	30	6	59.7	66.4	89.8	92.8	88.4	92.4	91.9	94.7
12	3	20	4	52.0	59.3	83.9	83.1	78.7	78.5	75.4	76.3
13	3	35	4	58.2	62.8	85.2	78.4	80.6	73.7	90.7	73.0
14	3	20	4	52.0	59.3	83.9	83.1	78.7	78.5	75.4	76.3
15	5	10	2	43.8	52.0	79.1	74.5	56.1	53.9	63.9	56.8
16	3	5	4	6.8	12.9	70.0	19.8	10.3	17.1	15.4	13.7
17	3	20	1	49.0	62.5	81.5	84.9	78.3	79.7	81.1	76.5
18	5	30	2	60.0	86.7	86.5	89.6	90.1	91.8	98.4	103.3
19	3	20	4	52.0	59.3	83.9	83.1	78.7	78.5	75.4	76.3
20	6	20	4	58.0	75.2	93.3	93.5	84.1	83.5	92.0	97.2

Note: ^a – actual values of response (dependent variables); ^b – predicted values of response (dependent variables).



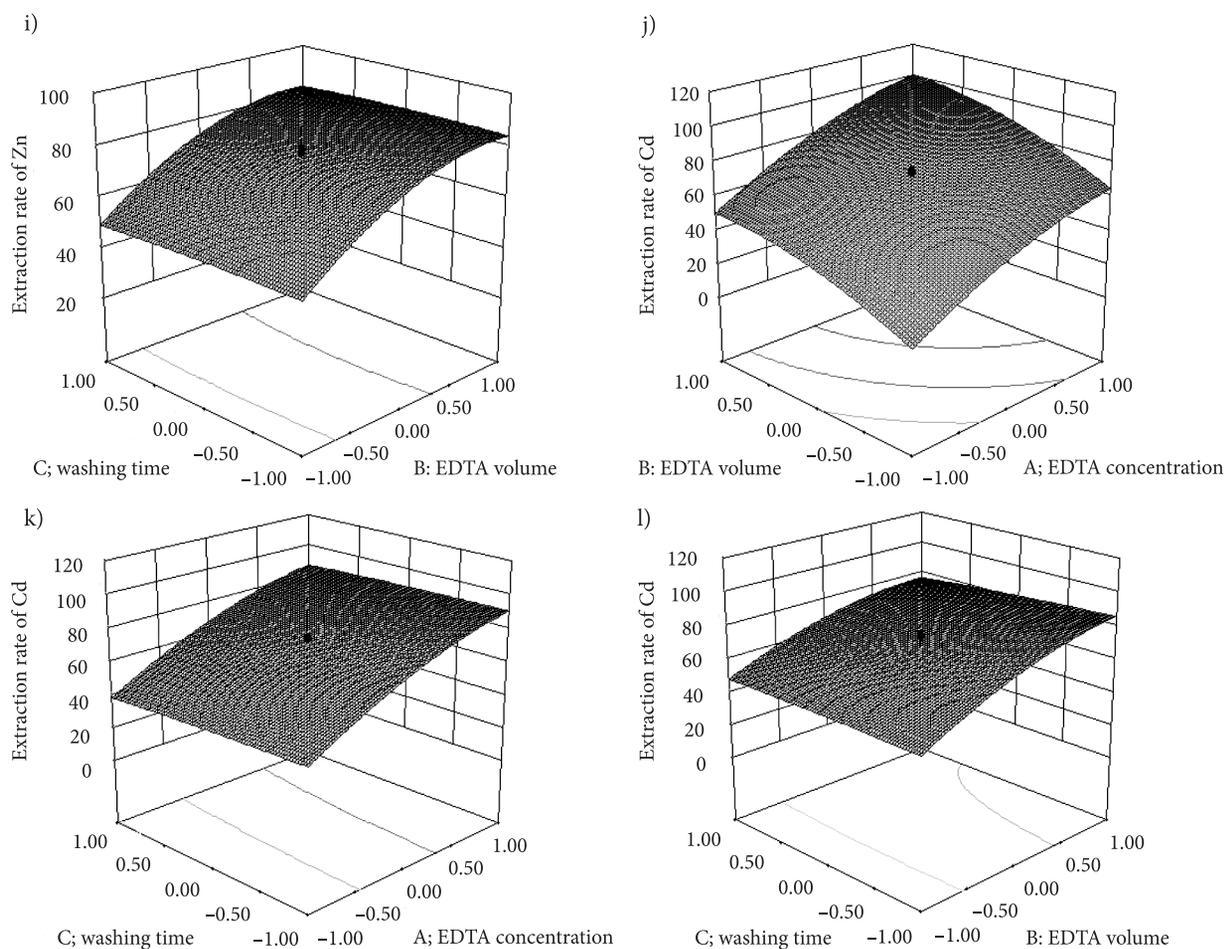


Figure 2. 3D surface showing the interaction effects of variables on extraction rates of various HMs: a) 3D surface of extraction rate of Cu and interaction of AB; b) 3D surface of extraction rate of Cu and interaction of AC; c) 3D surface of extraction rate of Cu and interaction of BC; d) 3D surface of extraction rate of Pb and interaction of AB; e) 3D surface of extraction rate of Pb and interaction of AC; f) 3D surface of extraction rate of Pb and interaction of BC; g) 3D surface of extraction rate of Zn and interaction of AB; h) 3D surface of extraction rate of Zn and interaction of AC; i) 3D surface of extraction rate of Zn and interaction of BC; j) 3D surface of extraction rate of Cd and interaction of AB; k) 3D surface of extraction rate of Cd and interaction of AC; l) 3D surface of extraction rate of Cd and interaction of BC

rate of Cu were EDTA concentration, solid-to-liquid ratio and oscillation time.

These facts are illustrated in Figure 2 (a–c). The tendencies of the extraction rates influenced by different factors are reflected by the curved surface. The interaction of factors are illustrated by the shape of the contour lines, an elliptical nature of the contour line indicated a significant interactions, while a circular contour line indicates the interaction between the corresponding variables is not significant (Francis et al., 2003; Yin, You, & Jiang, 2011). As the 3D surface graph shows in Figure 2, the extraction rate of Cu increases obviously with the increase of EDTA volume and concentration, while the change with oscillating time is unapparent. There is a significant interaction between EDTA volume and concentration, while interactions between other factors are not significant.

(b) Regression model analysis of extraction rate of Pb. The second-order polynomial regression equation

showing the relationship between the Pb extraction rate (Y_2) and three test variables is presented in Eq. (2):

$$Y_2 = -123.61689 + 48.09676 \times A + 9.79840 \times B - 2.83173 \times C - 0.59945 \times A \times B + 0.20523 \times A \times C - 3.65177E - 0.04 \times B \times C - 3.71889 \times A^2 - 0.15108 \times B^2 + 0.32478 \times C^2, \quad (2)$$

where Y_2 is the extraction rate of Pb; A is the concentration of EDTA solution ($10^{-3} \text{ mol} \cdot \text{L}^{-1}$); B is the solid-to-liquid ratio; C is the time of oscillation.

The ANOVA results for Y_2 were shown in Table 4. The ANOVA result of the regression model showed that the model is statistically extreme significant at the 95% confidence level ($P < 0.001$). There is no evidence of lack of fit. The coefficient of determination (R^2) was calculated to be 0.96, which means that the model could explain 96.33% of the values in the experiment, this result also proved a strong prediction of the model towards the response.

Table 4. ANOVA for the reduced quadratic model (Eq. 2)

Source	df	SS	MS	Prob>F
Model	9	2371	59	<0.0001
A	1	10680	265	<0.0001
B	1	4779	119	<0.0001
C	1	7	0.17	0.6849
AB	1	1149	29	0.0003
AC	1	5	0.13	0.7220
BC	1	0	0	0.9975
A2	1	2280	57	<0.0001
B2	1	2352	58	<0.0001
C2	1	17	0.43	0.5257
residual	10	40		

For Y_2 , two main factors (A, B), one interaction term (AB), and two second order factors (A^2 , B^2) were significant ($P < 0.05$). It indicated that the extraction rate of Pb was significantly influenced by EDTA concentration and solid-to-liquid ratio. The order of factors that affected the extraction rate of Pb were EDTA concentration, solid-to-liquid ratio and oscillation time. These facts are illustrated in Figure 2 (d–f), the extraction rate of Pb increases obviously with the increase of EDTA portion and concentration, while the change with oscillating time is unapparent. There is a significant interaction between solid-to-liquid ratio and EDTA concentration, while interactions between other factors are not significant.

(c) Regression model analysis of extraction rate of Zn.

The second-order polynomial regression equation showing the relationship between the Zn extraction rate (Y_3) and three test variables is presented in Eq. (3):

$$Y_3 = -71.39814 + 27.21643 \times A + 7.75242 \times B - 1.27599 \times C + 2.86458E - 003 \times A \times B + 0.21988 \times A \times C - 7.47648E - 004 \times B \times C - 2.94314 \times A^2 - 0.14681 \times B^2 + 0.044762 \times C^2, \quad (3)$$

where Y_3 is the extraction rate of Zn; A is the concentration of EDTA solution ($10^{-3} \text{ mol}\cdot\text{L}^{-1}$); B is the ratio of solid-to-liquid; C is the time of oscillation.

Table 5. ANOVA for the reduced quadratic model (Eq. 3)

Source	df	SS	MS	Prob>F
Model	9	1520	95	<0.0001
A	1	5507	343	<0.0001
B	1	4444	276	<0.0001
C	1	4	0.23	0.6408
AB	1	0.03	0	0.9686
AC	1	6	0.38	0.5489
BC	1	0	0	0.9918
A2	1	1428	89	<0.0001
B2	1	2221	138	<0.0001
C2	1	0.33	0.02	0.8889
residual	10	16		

The ANOVA results for Y_3 were shown in Table 5. Results showed the model was statistically highly significant at the 95% confidence level ($P < 0.001$). There was no evidence of lack of fit. The coefficient of determination (R^2) was calculated to be 0.9769, which means that the model could explain 97.69% of the values in the experiment. The effect of A, B, A^2 , and B^2 are extremely significant to the model in this case ($P < 0.001$). There is no interaction in any pair of factors. EDTA concentration and solid-to-liquid ratio were the main influence factors of Zn extraction rate. In contrast, the influence of the elution time was not significant. The order of factors that affected the extraction rate of Zn were EDTA concentration (A), solid-to-liquid ratio (B) and oscillation time (C). These facts are illustrated in Figure 2 (g–i), the extraction rate of Zn increases obviously with the increase of EDTA portion and concentration, while the change with oscillating time is unapparent. The interactions between factors are not obviously.

(d) Regression model analysis of extraction rate of Cd.

The second-order polynomial regression equation showing the relationship between the Cd extraction rate (Y_4) and three test variables is presented in Eq. (4):

$$Y_4 = -82.88057 + 22.58487 \times A + 8.11971 \times B + 3.80610 \times C + 0.059669 \times A \times B + 0.053288 \times A \times C - 0.11628 \times B \times C - 1.89104 \times A^2 - 0.14648 \times B^2 - 0.34270 \times C^2, \quad (4)$$

where Y_4 is the extraction rate of Cd; A is the concentration of EDTA solution ($10^{-3} \text{ mol}\cdot\text{L}^{-1}$); B is the ratio of solid-to-liquid; C is the time of oscillation.

Table 6. ANOVA for the reduced quadratic model (Eq. (4))

Source	df	SS	MS	Prob>F
Model	9	1762	16	<0.0001
A	1	7995	76	<0.0001
B	1	4872	46	<0.0001
C	1	61	0.58	0.4651
AB	1	11	0.11	0.7488
AC	1	0.36	0	0.9543
BC	1	43	0.41	0.5357
A2	1	590	6	0.0394
B2	1	2211	21	0.0010
C2	1	19	0.18	0.6769
residual	10	105		

The ANOVA results for Y_4 were shown in Table 6. Results showed the model was statistically extremely significant at the 95% confidence level ($P < 0.001$). There is no evidence of lack of fit. The coefficient of determination (R^2) was calculated to be 0.8795, which indicated a prediction of 87.95% of the experimental values. The effects of A and B are extremely significant ($P < 0.001$), and B^2 is significant to the model in this case ($P < 0.05$). There

is no interaction in any pair of factors. The results indicated that EDTA concentration and solid-to-liquid ratio were the main influence factors of Cd extraction rate. In contrast, the influence of the elution time was not significant. The order of factors that affected the extraction rate of Cd were EDTA concentration (A). Solid-to-liquid ratio (B) and oscillation time (C). These facts are illustrated in Figure 2 (j–l), the extraction rate of Cd increases obviously with the increase of EDTA portion and concentration, while the change with oscillating time is unapparent. The interactions between factors are not obvious.

The 3D response surface images are also in accordance with ANOVA results, which facilitate the overview of the interactions between two variables and their respectively impact for the extraction rate (Figure 2).

2.4. Validation of the model

Validation of the model was carried out by analysing experimental result under conditions predicted by the software. In this case, we set the extraction rate of Cu

reaching to 50% as the objective of EDTA-enhanced soil washing, 30 runs of combinations were given by Design Expert, the predicted conditions run by the software are in Table 7. Through experimental validation of the runs of 15 and 20, the predicted and the actual (experimental) responses of the extraction rate of Cu (49.2% and 51.5%) were comparable, which inhibited a good correlation between the experimental and the predicted values, and hence, the model was successfully validated.

In practical application, single-factor experiment and optimization by RSM method could be used in fitting out the heavy metal removal model. The optimal combination of parameters could be obtained by setting appropriate objective. Additionally, practical conditions such as relationship between EDTA concentration and solid-to-liquid ratio should be given overall consideration to reach a best balance between cost and efficiency under the premise of achieve repair purpose.

Conclusions

This work illustrates the feasibility of EDTA-enhance soil washing for multiple HMs contamination in the soil. Moreover, CCD and regression analysis method were proofed to be practicable and valid in determining the optimized combinations of soil washing conditions whilst maintaining economical technical parameters with high extraction rate. This approach is competitive in treating soil contamination with other types of pollutants for evaluating technical parameters fast and effectively, and of lowest cost.

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Disclosure statement

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Table 7. Simulating data sheet by Design Expert

Run	EDTA concentration / 10^{-3} mol·L $^{-1}$	EDTA volume /mL	Oscillating time /h	Extraction rate of Cu/%
1	4.25	14.3	3.81	50
2	2.08	26.2	5.89	50
3	2.21	26.2	2.86	50
4	2.00	29.1	4.55	50
5	2.52	22.0	4.07	50
6	2.00	28.2	5.24	50
7	3.63	16.0	5.77	50
8	2.44	23.2	2.97	50
9	3.73	16.2	2.28	50
10	2.38	24.0	2.76	50
11	2.57	21.3	5.12	50
12	2.27	24.5	3.72	50
13	3.25	17.5	5.72	50
14	3.11	18.3	3.68	50
15	2.50	21.8	5.23	50
16	2.02	27.9	4.69	50
17	3.61	16.1	5.09	50
18	2.18	24.8	5.42	50
19	3.65	15.9	5.28	50
20	2.00	28.5	4.92	50
21	4.58	13.6	3.49	50
22	3.39	17.3	2.65	50
23	2.70	21.2	2.75	50
24	2.21	26.2	2.89	50
25	3.24	17.5	5.68	50
26	4.35	14.0	5.61	50
27	4.42	13.8	4.34	50
28	3.69	16.0	3.38	50
29	3.33	17.5	2.97	50
30	2.53	21.6	5.43	50

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