

## ANALYSIS OF WATERPROOFING DEFECTS AND TECHNOLOGY DEVELOPMENT FOR CAR PARKING ROOFS: LITHUANIAN CASE

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**Abstract.** This work presents the analysis of installation options of exploitable car park roofs offered by the designers, material manufacturers and suppliers and introduces the Lithuanian legislation with the requirements for this type of roofing. Reasons of the most frequently occurring defects have been examined and several options for correcting defects have been provided. The most cost-effective option for correcting the defect in question has been chosen. Practical measures for increasing the reliability of exploitable car park roofs have been proposed. The analysis has shown that at a minimum slope reliability of the exploitable roof coated with roller heat-welded materials is not guaranteed. The authors propose to tighten the requirements on car park roofing.

**Keywords:** waterproofing, roof slope, exploitable roof, flat roof.

### 1. Introduction

Since congestion of vehicles in cities is constantly increasing, car parking problem is becoming more and more acute. Due to land scarcity and continual price increases parking lots turn into a multi-storey or underground structures (Milosavljevic *et al.* 2010). Therefore it is natural that attempts are made to exploit roofs of such buildings – they are becoming an additional space to keep vehicles or can be installed as a pedestrian zone. Strict requirements are applied for this type of roofing. Roof coating shall be watertight in order to prevent the roof structural elements from corrosion and erosion, be able to bear vehicle loads (Medeliene, Žiogas 2010), the roof spaces in use must be safe for traffic participants and, of course, be aesthetically attractive. Similar problems may arise while exploiting green roofs, which can be installed for both the aesthetic and economic reasons.

Currently, the industry can supply a wide range of different materials for waterproofing of flat roofs (Oba, Hugener 1995; Ogle *et al.* 2004; Baskaran *et al.* 2008, 2009; Baskaran, Molleti 2009). Their proper use may extend the durability of the roof to 30 years and more. But actually, after the start of exploitation of flat roofs with car parks installed on top, experts have been receiving many complaints about lack of credibility of such type of roofing. As it is known, the basic conditions for ensuring the reliability of the roof are the right design solution, the use of quality materials and rigorous compliance to technological requirements on roof installation.

Roof is the top covering part of the building, protecting its interior from atmospheric effects (STR 2.05.02:2008 2008). Walter *et al.* (2005) has classified

the most common defect types and causes. Although this work deals with exploitable roofs designed for car parks, but similar problems may arise when exploiting green roofs, which can be installed for both the aesthetic and economic purposes (Wong *et al.* 2003; Ismail *et al.* 2010). Gränne *et al.* (2003) tested the wind load resistance of joints between roofing felt and sheet metal and found that peeling is the dominating process in the failure of joints during wind load.

Based on extensive research, it was found that the greatest damage to structures has been caused by violations related to defective waterproofing. For example, tests performed in Sweden (Gränne, Björk 2000) show that it is possible to obtain joints with sufficient strength using the contractors ordinary welding procedures. In Norway, which is famous for high level of labour culture, the building defects related to waterproofing violations represent 41% of all defects (Lisø *et al.* 2005). It is likely that in Lithuania this percentage is even higher.

Currently, reduction of energy consumption is becoming a topical problem, which can only be achieved by proper installation of insulation layer, using appropriate materials (Rudbeck 2002). One of the most widely used thermo insulation building materials is expanded polystyrene. According to Vaitkus *et al.* (2006), exploitation of expanded polystyrene in most cases is related to compression deformations. Properties of such materials are directly dependent on the structure and shape of a pore or granule.

The most serious problem of glued roller cover materials for roofs is insufficient reliability of seams between the strips of glued membrane. Karablikovas (2007) was focused on the mechanism of seams formation and the determination of seams quality parameters – the

thickness of seam, the strength and unglued area of seam. Research indicates that using of bituminous heat-welded polymeric substances for installation of rolled flat roofs increased their durability. The research of this problem focused on the mechanism of seams formation and the impact of gluing technology on seams quality parameters – strength, thickness and emergence of unglued areas in the seam. The final seam thickness is regarded as an additional indicator and the research-based importance of this indicator has been presented. The dependence of adhesion strength on heating duration of melted surfaces has been proven experimentally. The research shows that the maximum strength of seams does not exceed 15–20% of the rolled cover material strength and can not be increased by applying the existing roof gluing technology. A series of practical measures for increasing the reliability of flat roofs bituminous membranes have been proposed. Later Karablikovas and Vilitienė (2010) made an analysis of the dependence of seam strength on heating duration of melted surfaces and provided the suggestions for glued roller roofing technologies. The dependence has been determined experimentally. The analysis had shown that the heating regime not ensures the necessary gluing level of membrane layers.

The aim of the Oba *et al.* (1996) study was to understand how the T-peel strength of heat-welded seams in polymer-modified bituminous roofing membranes depends on the welding method and on the material properties. It was concluded that the choice of welding speed and pressure weight for the optimum design of welding machine should make reference to the thermal properties, such as specific heat, and to the rheological properties, such as viscosity.

Fajkos (2007) tests had shown that temperature affects the overlap character of seams. Nil and Ertan (2004) argues that at the very wall waterproofing is exposed to the highest pressure. Under these conditions, the stresses caused in the coating reduce the thickness of the membrane, leading to an increased probability of water and vapour permeability. This effect is also relevant to bituminous coatings, as high compressive pressure can cause leakage through the seams. It has been estimated that the maximum strength of roof seams is 5–6 times smaller than the strength of roller material (Karablikovas 2007).

The satisfactory performance of a membrane waterproofing system, during its useful life, relies solely on the permeability of the waterproofing membrane, when construction and workmanship are correctly implemented. In field conditions, the membranes are subjected to various stresses, such as those brought about by building loads and lateral soil pressure that may strain the membrane, particularly in deep basements, and adversely affect its permeability. Nil and Ertan (2004) proposed a new performance-based laboratory test method to assess the vapour and water permeability of strained waterproofing membranes under hydrostatic pressure. The novelty of the method is that for a given basement configuration (height and depth), the effects of strain arising from tensile stress and compressive pressures acting on the membrane are simulated on the test specimen and the vapour

and water permeability is measured in laboratory conditions. The test results confirmed that at some strain levels that simulate field conditions, to which membranes can be subjected, the strained membranes transmitted vapour under hydrostatic pressure. The tests also revealed that the test apparatus was effective in measuring the vapour and water permeability of the specimens under hydrostatic pressure (Nil, Ertan 2004).

Performance of elastomeric waterproofing membrane depends not only on the material properties, but also on the quality of the installing equipment. Currently, among the products on sale there are cold, liquid, spreadable, self-adhesive elastomers, which differ in chemical composition and application methods. Application problems can emerge due to changes in atmospheric conditions, quality of work and surface preparation. Mailvaganam and Collins (2004) examined the interaction of quality of five elastomeric membranes with the quality of surface preparation. The results show that due to the poor quality of work performed and lack of control the final product is unstable.

Atkinson (2002) analyzed the impact of the managerial staff on emergence of defects. Research results confirmed that most of the defects occur due to insufficient performance of managerial staff, but this can also be attributed to random chain of events. Quite often wrong solutions of the managerial staff result in errors in subsequent work processes which lead to making incorrect conclusions followed by inappropriate actions. The study also proposes a conceptual model of the nature of an error in construction projects and shows that the defects result from the impact of management decisions thus, when investigating the causes of incidents organizations must be assessed in an integrated way.

Mailvaganam and Collins (1999) identified three main factors affecting the work of elastomeric membranes on the car park roofing: quality of installation, quality of ground preparation and environmental conditions. It is also important to comply with the manufacturer's instructions while carrying out the work.

The aim of this work is to identify causes of defects of the test car park, offer a rational option of failure correction and measures for installation of exploitable roofs in the future in order to increase their reliability.

## 2. Analysis of modern roofing construction

Currently, depending on the destination, flat roofs are made as non-exploitable and exploitable, latter furnished with terraces, flower gardens and swimming pools. Constructively roofs can be thermo insulated and non-insulated, ventilated and non-ventilated. Insulated roofs according to thermal insulation placed in the roof structure can be divided into *direct* or *reverse*. Despite this diversity, the main elements of flat roofs remain the same: supporting structure; vapour barrier; heat insulation with ventilated air space or without it; levelling layer; high-quality waterproofing coating that must remain leak-proof at long-term, withstand the extreme loads and serve as protective layer.

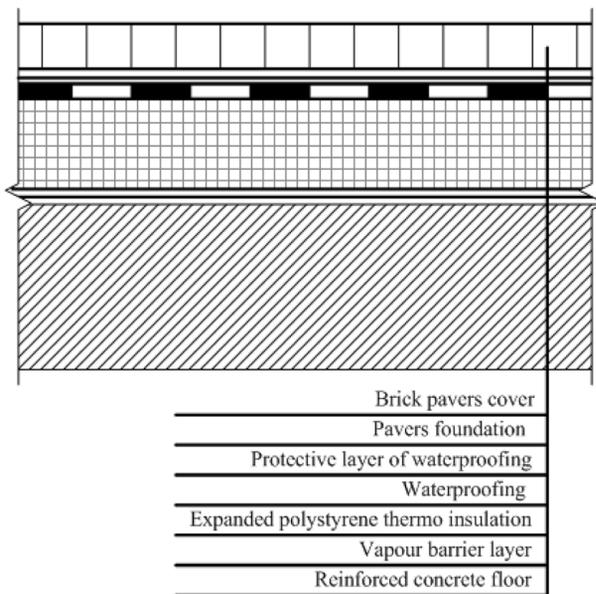


Fig. 1. Installation option of the direct exploitable roof

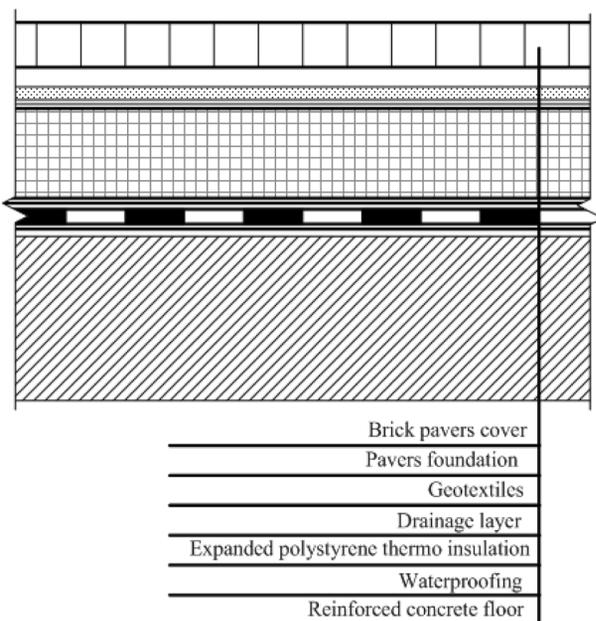


Fig. 2. Installation option of the reverse exploitable roof

*Installation Options of Exploitable Roofing.* The figures below presents the installation options of the exploitable roof: first – the direct exploitable roof, when the waterproofing layer is installed over the thermo insulation layer (Fig. 1); and second – the reverse exploitable roof, when waterproofing layer is installed under the thermo insulating layer (Fig. 2).

*Types of waterproofing.* The figures below present different classifications of waterproofing coatings (Gajauskas 2004): first – the classification according to the origin (Fig. 3), and second – according to the possible ways of fastening of waterproofing materials (Fig. 4). First classification (“by origin”) divides the waterproofing coatings into three main groups, i.e. roller roof coatings, membrane coatings and mastics. Waterproofing coatings could be

fastened by different ways: glued with special glues, mastics, by hot air; poured, sprayed, fastened mechanically, ballast-loaded and, finally, heat-welded.

### 3. Constructing roof slope

Reinforced concrete slabs are the basis of roofing. Reinforced concrete slabs must withstand the static and dynamic loads. Good water drainage is required in order to protect reinforced concrete slabs, thermo insulation, structures below and other assets from the adverse effect of water.

Reinforced concrete slabs are usually made of a monolithic and prefabricated reinforced concrete. Reinforced concrete slabs are calculated for the entire operational period, so the waterproofing coating together with the design of roof slope should ensure the operational longevity of structure.

The flat roofs are sensitive to cracking and leakage; therefore flat roofs must be designed so that water can drain off quickly from the roof surface. No exceptions can be allowed in designing a roof without slopes. One can often see water accumulation or swamps on the old roofs. This is due to the minor slope, therefore water causes additional threats and there is a risk that in the weakest areas water will penetrate and seep into the roof structure.

Typically the slope is achieved in the following ways:

- by installing bearing structures with a slope;
- with the help of levelling layer;
- using thermo insulation materials of a variable thickness.

Thermo insulation materials of a variable thickness are not used in roofs of a complex surface.

Minimum and maximum values of roof slope are regulated by the Construction Technical Regulations. The minimum allowable slope or grade of exploitable flat roofs in Lithuania is  $0.7^\circ$  (1.25%) (STR 2.05.02:2008 2008). To achieve quick water runoff from such roof, the designer must estimate the possible inaccuracies and deformations during the installation and installer must avoid the fitting errors. If latter occur, slope decreases and properties of flat roof become worse (Fig. 5).

After increasing the slope twice, theoretically it becomes  $1.4^\circ$  (2.5%), but in practice due to a possible sags the slope becomes at an average around  $0.7^\circ$  (1.25%) (Fig. 6).

When choosing a minimum slope after the evaluation of possible deflections, it is necessary to pay attention to sags in the roof structure which can have either a positive (Fig. 7) or negative impact on water runoff (Fig. 8).

After the installation of roof drain in the mid-span, the sag improves water runoff (Fig. 7). However, in most cases, roof drains are installed near walls or columns, and then the sag usually worsens the runoff (Fig. 8). When choosing the roof slope, it is necessary to take into account the following conditions:

- when forming a slope with a levelling layer, the construction sag is filled with the levelling substance, so the slope becomes constant;

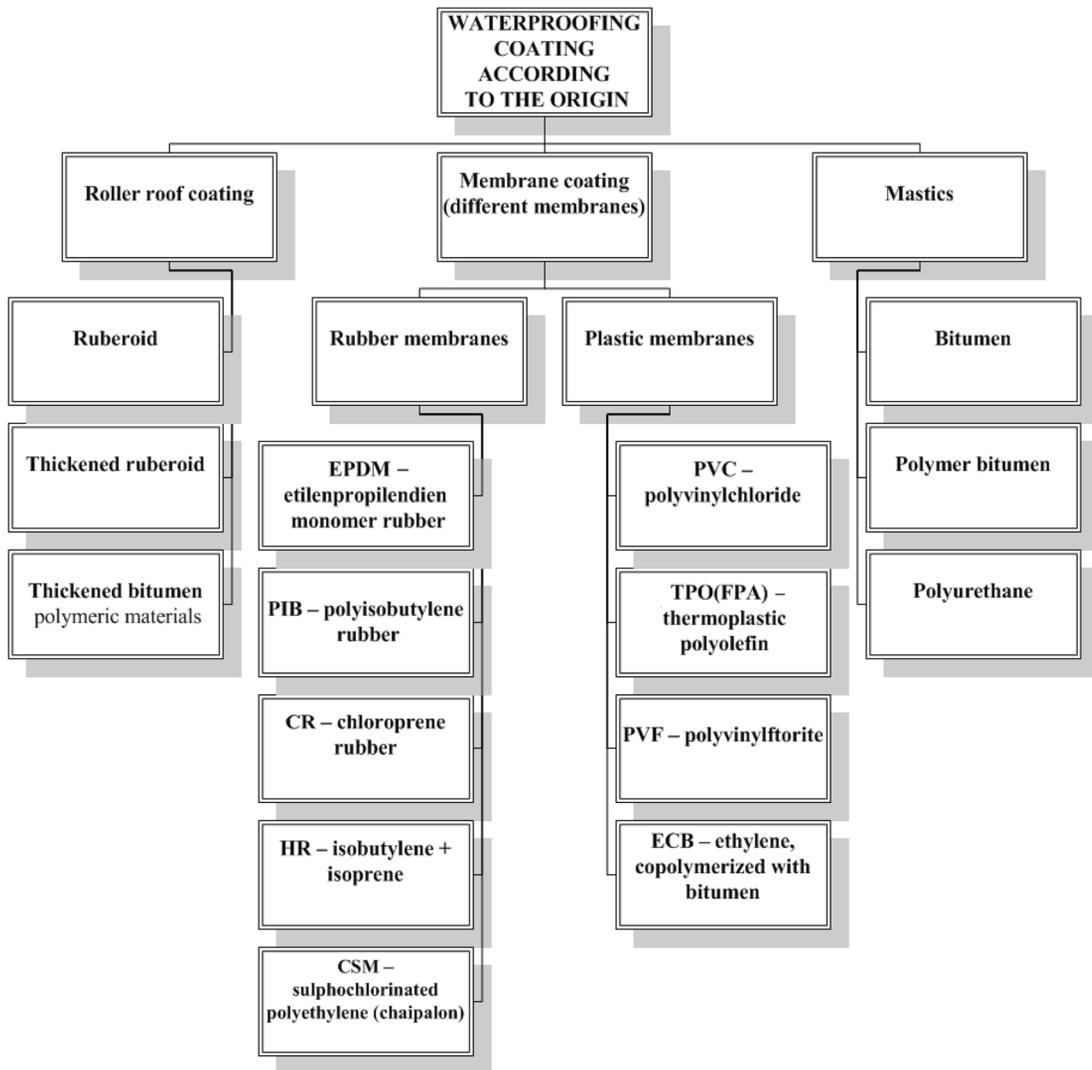


Fig. 3. Classification of waterproofing coatings by origin

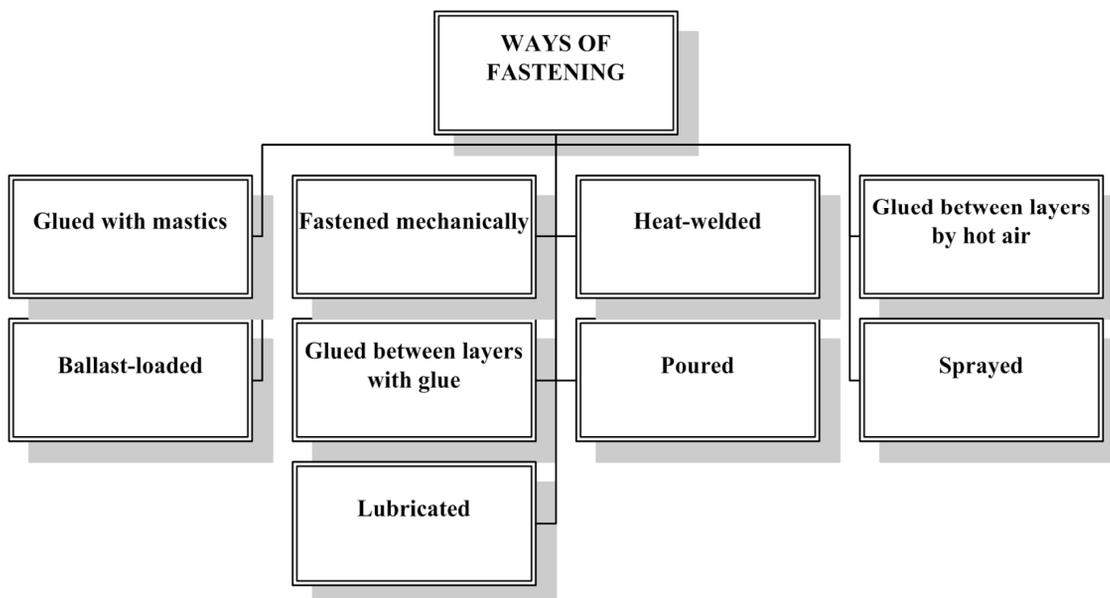


Fig. 4. Classification of waterproofing coatings by way of fastening



Fig. 5. A scheme showing a reduced slope due to fitting errors (slope 1:80)



Fig. 6. A scheme showing the formation of swamps due to fitting errors (slope 1:40)



Fig. 7. A scheme showing how the sagging in the roof improves the runoff

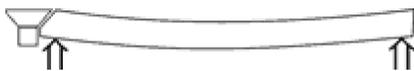


Fig. 8. A scheme illustrating how the sagging in the roof worsens the runoff

- at the junction of two slopes of different directions a confluence may arise and its effectiveness gets smaller than that of the basic area.

Let us examine the situation where the designed marginal slopes of the roof base are  $0.7^\circ$  (1.25%). The designers often do it because of large parking areas and restricted possibilities to thicken the roof structure. In this case, the slope of the roof at the confluence will be only  $0.5^\circ$  (0.88%) (Fig. 9). However, this doesn't comply with requirements (STR 2.05.02:2008 2008).

Layout possibilities for rain water gutters, installed inside and generally located near the main supports, as well as for roof drains, are often limited. Despite that fact, roof drains should be installed in way to ensure the adequate slopes of the roof surface. The slopes in such case should ensure the water runoff both in perpendicular and diagonal directions in respect of the roof sides (Fig. 9).

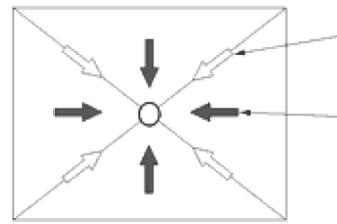


Fig. 9. Scheme of junction of roof slopes in place of rain water gutters

Particular attention should be given to the installation of water drainage layer. If the roof slope is correct, but water can not run off freely, sooner or later will appear the problem of water leakage.

There are three options for installing roof flashing: different mastics, membrane coatings and bituminous polymeric roller heat-welded or glued by a variety of roofing mastics. This article analyses only roller roofing most often used for flat roofs.

The main criteria that determine the quality of roof installation are as follows:

- exploitable flat roof slope must be at least  $0.7^\circ$  and not more than  $7^\circ$ ;
- for roofs with a slope of  $0.7^\circ$  to  $1.4^\circ$ , the specially designed construction products and structural solutions according to the manufacturer's recommendations on installation of waterproofing cover have to be used;
- flat roof slope to the roof drain must be at least 1.4 (STR 1.05.06:2010 2010).

For the analysis of slope installation efficiency, a roof of  $10 \times 10$  meters in size, whose central part is equipped with a water drain, has been chosen. The main gradient to the drain of the analyzed roof makes 2.5%, the roof cover is not specifically designed for small gradients. It is assumed that the maximum roof seam strength is 5–6 times lower than the roller material strength (Karablikovas 2007). Let's analyze three possible options for formation of roof slopes with the drain in the centre (Fig. 10).

A case showed in Fig. 10a, when the roof is divided by two diagonals into four zones of triangular shape and water runoff is evenly directed to the same drain has been examined and presented Fig. 11. Suppose that the slope is

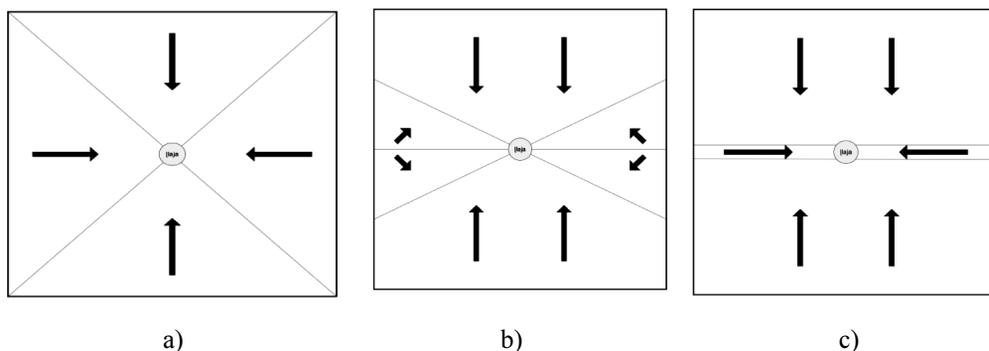


Fig. 10. Possible options for formation of the roof slopes: a) all the same slopes; b) composite slopes; c) confluence in the middle

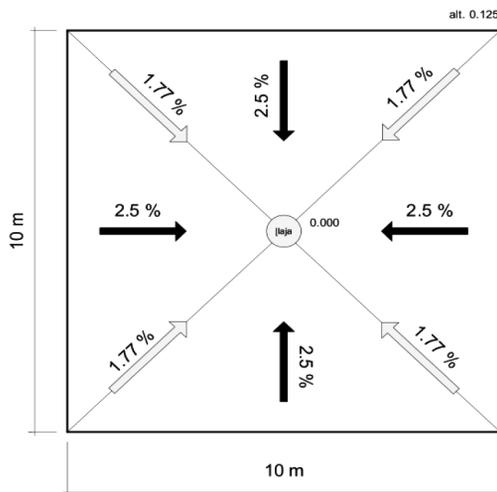


Fig. 11. The roof slopes model

2.5% (black arrow), roof dimensions are 10×10 m, the drain is at 0.000 (zero) altitude. The present research does not take into account that within the radius of 0.5 m from the centre of the vertical drain roof surface must have at least 6° slope to the roof drain and the altitude of the edge must be 0.125 (STR 2.05.02:2008 2008). Then the slope of the roof at the intersection of roof zones is only 1.77% (white arrow). This type of roof slope is only possible when using construction products and structural solutions specially designed for such roof slopes.

When designing flat roofs designers should consider the fact that the most commonly used type of welding devices in Lithuania are gas burners, but they can not adjust to the welding speed or clamping force, therefore it can be argued that the heat-welding of the roller cover is not a sufficiently controlled process. The only way to ensure the control is a streak of molten bitumen mass in a formed seam. The earlier researches (Karablikovas 2007) found that the strength of seams is mainly poor; therefore the fact that heat-welded roller roof covers can be used for exploitable roofs becomes questionable. There is a substantial risk that a roof with such a low gradient can start to leak due to the complicated water runoff and water accumulation at intersections.

A case showed in Fig. 10b has been examined and presented in Fig. 12. Under the same initial conditions it is not possible to raise all edges of the roof to the proper altitude (0.125), but the required slope of the roof zones (2.5%) is maintaining (Fig. 12). In this scheme the slope at the intersection of the zones is only 1.1% (white arrow), which does not comply with requirements (STR 2.05.02:2008 2008).

In areas where the lack of the necessary degree of roof slope appear an additional waterproofing layer is required, but even this measure can not provide the full tightness of the roof against water.

When designing roofs the marginal slopes should be excluded and slopes of roof zones' intersections should be evaluated strictly (Gajauskas 2004). Fig. 13 provides the theoretical scheme of the roof, which has already met all the minimum requirements of construction technical regulations, here the slope at the intersections of roof zones

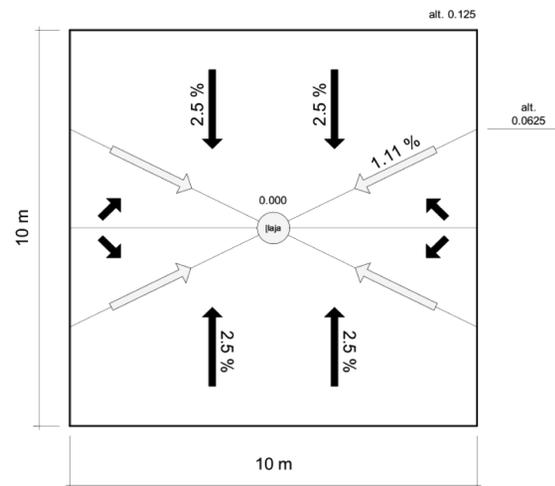


Fig. 12. Roof slope model, when the height of one or two opposite edges of the roof is limited

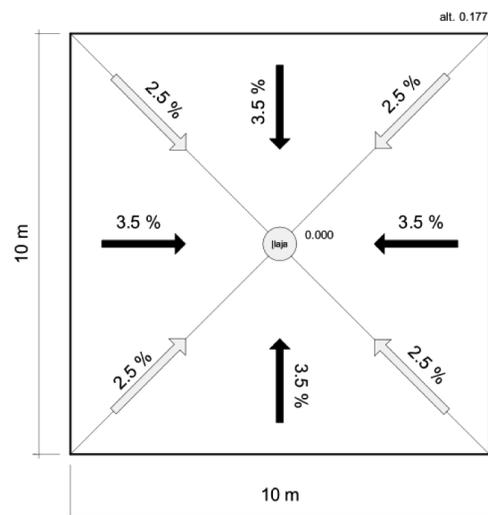


Fig. 13. The model of roof slopes and the slope size, which meets all the minimum (STR 2.05.02:2008 2008) requirements

is 2.5% (white arrows). It is recommended to start designing the roof from the intersections and only then to select the slope for other zones of the future roof.

The presented model suggests the roof slopes where the gradient of the main zones has to be 3.54%, but the simulation has been adopted in ideal conditions. The possibilities of deviations in building structures (flooring, levelling layer or gradient formation) during construction and deformations of the building during its exploitation were not taken into account. Water drainage layer ("honeycomb" type or other) has also been underestimated, because the waterproofing layer of exploitable roofs is inside the roof structure. The present analysis indicates that currently the slopes in designed main roof zones are not sufficient. It is proposed to pay a special attention to the formation of slope at the intersections of roof zones when designing roofs, and in particular the exploitable ones. After assessment of poor durability of the roller heat-welded cover seams, it is recommended not to use them in exploitable roofs, but rather replace them with the membrane coatings or the similar.

#### 4. Defects analysis of a car park in Vilnius

While carrying out the analysis of defects in waterproofing, a car park building located in Vilnius, which has all the characteristic features and consequences resulting from violation of waterproofing, was studied. It was not determined if the construction work in the analyzed object was carried out in accordance with the technical requirements of the project, because unfortunately, it was not possible to find the description and installation requirements of the car park roofing layers. The surface layer of the underground parking has been covered with scotch blocks and pavement tiles.

The survey showed that actually the car park roofing has been accomplished according to the scheme shown in Fig. 14.

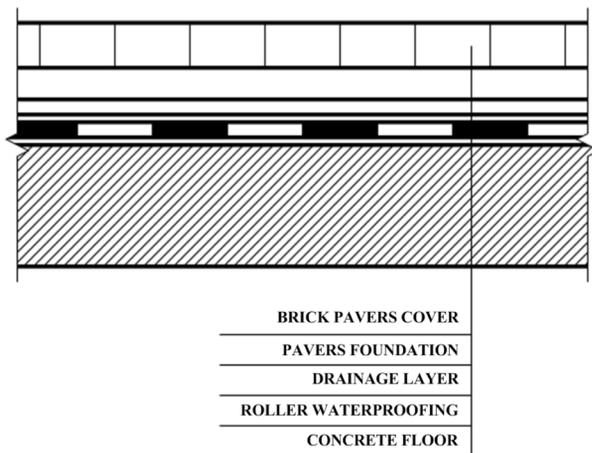


Fig. 14. Section of car park roofing

The inspection revealed that:

- there is water penetration at transoms in the car park;
- moisture penetrates through the walls of car park;
- patches of moisture penetration was observed through the floors of car park;
- there is penetration of water at the junction between the wall and floor;
- there is no flashing (weatherproofing) on the outside of the building at the basement level;
- the outer walls of the car park are not hydro insulated below the zero level.

The inspection revealed that the outer moisture gets into the basement premises of the car park. Moisture leakage causes damages to the building structures, equipment as well as to the property inside it. During the research analysis on moisture presence in the car park was carried out. Internal car park general indoor measurements were performed, the following parameters were registered:

- internal temperature: +19.62 °C;
- water concentration in air: 9.3 (g/m<sup>3</sup>);
- the average relative air humidity: 66.0%;
- dew point temperature: +13.1 °C.

Humidity measurements of car park construction up to 4 inches deep and thermo visual analysis of individual sites were performed.

It was found that water penetrates into the building structures due to an insufficient slope directing water from the car park roof, improper installation of exploitable roofing, absence of the draining layer. Since the easiest way for water to get inside is through the junctions/intersections of the building structures, first of all water penetration appears in these places (Fig. 15). Considering the above findings it is concluded that the construction work on installation of the car park does not meet the normative quality requirements.

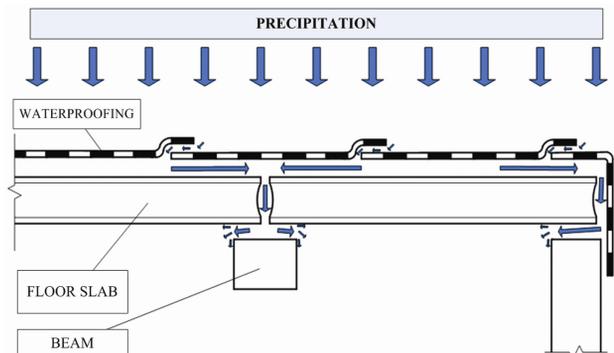


Fig. 15. Scheme of moisture entering the car park

#### 5. Alternatives for recovery of waterproofing layer of car park

The study showed that the object under analysis lacks the slope formation layer beneath the waterproofing layer. This does not comply with the requirements of STR 2.05.02:2008 (2008) clause 35.2. According to the requirements an additional roof waterproofing layer and a layer designed for draining the flashing water are mandatory, but actually only one roller cover layer has been installed. The object under study has not been equipped with water draining layer and additional waterproofing layer. One waterproofing layer can not ensure watertightness due to unreliable seams of the roller cover. The research (Karablikovas 2007) shows that possibilities of increasing the adhesion strength of roller cover stripes by prolonging the heating time are limited and insufficient. To ensure the reliability of roofing from heat-welded materials it is proposed to tighten the requirements on the roof construction.

Therefore, to prevent water leakage in the future, additional waterproofing layer must be installed for the elimination of the defects under this study.

The study determined that the car park walls do not have vertical insulation from the outside, which results in water permeability of the mentioned walls.

After the assessment of waterproofing defects and their extent at the car park, two alternatives for reconstruction of waterproofing layer have been offered.

*Alternative A<sub>1</sub>.* An efficient and fast way to restore the waterproofing layer is to use resilient flashing mastic. Polyurethane waterproofing material with quartz sand filler is specifically designed to protect roadways with high vehicle loads against water, salt, oil and abrasion. The flashing mastic in use must be resistant to mechanical, chemical and thermal effects. It is used to form upper



**Table 1.** Initial decision making matrix

Indicators	Measuring units	Optimality direction	Significance, $q_i$	Alternatives	
				$A_1$	$A_2$
Price of 1 m <sup>2</sup> repair	Lt*/m <sup>2</sup>	min	0.219	77	116
Person-hours	hours	min	0.238	0.25	0.30
Repair duration	minutes	min	0.011	7	3
Longevity	years	max	0.389	7	5
Technological efficiency	points	max	0.083	5	7
Slope after repair	%	min	0.049	1.5	2.5
Aesthetic appearance	points	max	0.011	10	3

\* a basic monetary unit of Lithuania, containing 100 cents, 1 EUR = 3.4528 LTL (the exchange rate fixed by Lithuanian central bank)

**Table 2.** The results of calculation applying COPRAS method

Indicators	Optimality direction	Significance	Measuring units	Alternatives	
				$A_1$	$A_2$
Price of repair	min	0.219	Lt/m <sup>2</sup>	0.087	0.132
Person-hours	min	0.238	hours	0.108	0.130
Repair duration	min	0.011	minutes	0.008	0.003
Longevity	max	0.389	years	0.227	0.162
Technological efficiency	max	0.083	points	0.035	0.048
Slope after repair	min	0.049	%	0.018	0.030
Aesthetic appearance	max	0.011	points	0.008	0.002
Weighted sums of normalized maximizing criteria of the alternatives $S_{+j}$				0.269	0.213
Weighted sums of normalized minimizing criteria of the alternatives $S_{-j}$				0.222	0.295
Significances of the alternatives $Q_j$				<b>0.565</b>	<b>0.435</b>
Priorities of the alternatives				<b>1</b>	<b>2</b>

- R3 – 1 m<sup>2</sup> repair duration (in minutes);
- R4 – longevity of performed repairs (years);
- R5 – technological efficiency (points);
- R6 – roof slope after repair (%);
- R7 – aesthetic appearance (points).

Alternatives with indicators' values and significances are presented in Table 1.

Table 2 presents calculations done by applying COPRAS method. The variants have also been compared by applying TOPSIS and SAW methods. Assessment results of analyzed alternatives ( $A_1$  and  $A_2$ ) are presented in Table 3.

**Table 3.** Aggregated results of analyzed alternatives

Method	Alternative	
	$A_1$	$A_2$
TOPSIS	0.851 (1)	0.149 (2)
SAW	0.970 (1)	0.749 (2)
COPRAS	0.565 (1)	0.435 (2)
Rank	1	2

According to the values received in determining the rationality of alternatives, a conclusion follows that  $A_1$  is a rational variant. Since the rationality of variants after application of the three methods totally coincides, we have not continued calculations with other methods provided in the methodology set MCDM for a case when variant rationalities do not coincide (Ustinovichius, Zavadskas 2004).

## 7. Conclusions

Lithuanian and foreign experience in roofing installation and requirements of Lithuanian legislation on of exploitable roofs has been analyzed. Analysis revealed the positive and negative features of flat roofs. In order to ensure the good performance of flat roofs it is suggested:

1. When designing flat roofs a special attention should be focused on the slopes of roof zone intersections. It is recommended to start designing the roof from the intersections and only then to select the slope for other zones of the future roof. This way would increase the reliability of design solutions.

2. When installing flat roofs a strict control of work performance should be ensured. By analyzing the defects of the exploitable car park roofs it was found that typical non-conformities can be classified as non-compliance with construction requirements and violation of technological process requirements.

3. The analysis of case study object has been performed. Two alternatives for the reconstruction of waterproofing coating in order to ensure roof tightness have been offered. Multicriteria analysis of roof waterproofing alternatives has been carried out. It has been determined that the rational alternative for the removal of existing defects is  $A_1$  alternative flooring system.

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