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## MONITORING OF MASJED-SOLEIMAN EMBANKMENT DAM'S DEFORMATION USING A COMBINATION OF INTERFEROMETRIC SYNTHETIC APERTURE RADAR (INSAR) AND FINITE ELEMENT MODELING

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**Abstract.** The fresh water shortage is one the most important challenges in many countries like Iran. So there have been incentives to manipulate and manage water resources by constructing dams. Clay core embankments are one of the most popular dam structures. A layer of clay can be a reliable obstacle in front of water stream. However, because of the soil's nature, these kinds of dams have the potential of instability. Thus deformation of clay core dams should be monitored frequently. The aim of this study is to use the combination of Interferometric Synthetic Aperture Radar technique (InSAR) and Finite Element Modeling (FEM) for dam's deformation monitoring. For the InSAR analysis we used data from ENVISAT sensor and processed those using Small BAseline Subset (SBAS). We show that InSAR is an invaluable approach to monitor clay core dam's deformation in specific circumstances. The deformation derived from InSAR was used as an initial condition in Finite Element Modeling. The case study is Masjed Soleiman Dam which is situated in South West of Iran. We used 19 ASAR images of ENVISAT sensor from 2003/8/22 to 2010/5/7. The process of ASAR images showed maximum velocity of 11 mm/year in LOS direction at central lower areas of dam. These results were compared with Geodetic Surveying Operations at four points on dam and the average agreement of 77 percent was obtained. The results of ENVISAT data have a good consistency with FEM results. Horizontal and vertical displacements derived from instrumentations and modeling are plotted versus depths. There is a good agreement between modeling results and instrumentations data.

**Keywords:** insar, finite element modelling, deformation, embankment.

### Introduction

Since any failure in embankments leads to enormous financially and human losses, frequent deformation monitoring of embankments is vital and inevitable. There are a wide variety of approaches for structure monitoring including conventional geodetic operation, close range photogrammetry, laser scanning and global positioning system. However, due to spectacular features like all weather and time measurements, high spatial resolution and comprehensive data collection, InSAR could be a reliable and powerful tool to observe structures movements. In addition, this method does not require direct contact with construction. So, several works concerning the InSAR capability of deformation monitoring have been put forward (Luo *et al.* 2011; Honda *et al.* 2012; Perissin *et al.* 2009; Wang

*et al.* 2011; Monells *et al.* 2010; Hooper *et al.* 2012; Voege *et al.* 2012; Di Martire *et al.* 2014; Milillo *et al.* 2016; Shamshiri *et al.* 2014).

Embankment dam modeling empowers engineers to predict dam behavior under loadings like water force, dam weight and consolidation phenomena. Also they can determine the source of dam failure to take immediate actions. In this study obtained displacements of InSAR method have been imported as an initial condition in modeling.

Initially 19 ASAR images of ENVISAT sensor between years 2003 and 2010 have been employed. The wavelength of images is 56 millimeter and incidence angle is approximately 23 degrees. The SBAS method implemented in StaMPS software (Hooper *et al.* 2012) have been used to acquire time series deformation.

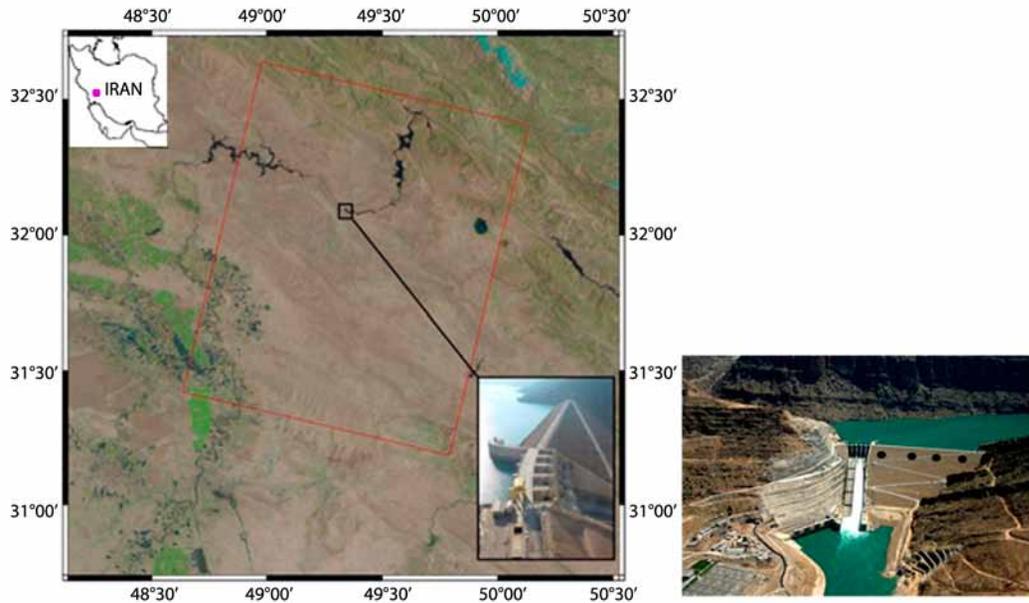


Fig. 1. Masjed Soleiman Dam, it's Location, SAR image frame and geodetic points of Figure 2 (black points)

Due to poor quality and correlation, 6 images between years 2003 and 2004 were processed ultimately.

Since Karoun River is the longest river (950 km) of Iran and has the highest level of water, notable number of dams has been constructed along it and Masjed Soleiman Dam is one of them. Masjed Soleiman Dam is a hydropower dam which is located south west of Iran in Masjed Soleiman City. Construction of dam was finished in year 2000 and was operated in that year. This dam is capable of producing 2000 MW electricity now. Catchment basin of dam is 25829 km<sup>2</sup> and its elevation is 177 meter from foundation and 172 meter from riverbed. Dam crest is 15 meters wide and 488 meters long. Masjed Soleiman dam is a clay core dam (Fig. 1).

## 1. Methodology

### 1.1. Time series extraction by SBAS

The SBAS implemented in StaMPS has been used in this study. The network was obtained by pair images with these conditions: time interval less than 1500 day, perpendicular baseline less than 1050 meters and coherence greater than 0.35.

The phase noise can be estimated from the interferometric SAR pair by means of the local coherence. The local coherence is the cross-correlation coefficient of the SAR image pair estimated over a small window. The coherence value ranges from 0 (the interferometric phase is just noise) to 1 (complete absence of phase noise) (Ferretti *et al.* 2007).

Instability of scatterers, incidence angle and antenna pattern deviation of squint result in decorrelation. Therefore, the time differences of pairs must be as minimum as possible to minimize the decorrelation of scatterers instability (Hooper 2006, 2008). Decorrelation of squint and incidence angle deviation could be minimized by means of a suitable band pass filter. SBAS method is looking for Slow Varying Filtered Phased (Hooper 2008).

Processing steps are as follows:

First of all, a network of appropriate interferograms is constructed. It should be mentioned that all images are filtered in range and azimuth direction to remove geometric decorrelation and non-overlapping part of Doppler spectrum. So the coherence of pixels will be maximized (Hooper 2008; Kampes *et al.* 2003).

SBAS is interested in pixels with negligible phase due to non-spatial decorrelated term of noise. Spatially correlated terms are estimated by using a band pass filter. Also non-spatial decorrelated term of DEM error is proportional to perpendicular baseline. Consequently, non-spatial decorrelated term of noise could be calculated simply (Hooper 2006).

In order to reduce calculations and accelerate process, phase instability ( $\gamma$ ) of pixels with small Amplitude Dispersion Index (ADI) is estimated:

$$\gamma = \frac{1}{N} \left| \sum_{i=1}^N e^{i(\varphi_{\text{int}} - \tilde{\varphi}_{\text{int}} - \Delta\varphi_{\text{DEM}}^{\text{NC}})} \right|. \quad (1)$$

$N$  denotes the number of interferograms,  $\tilde{\varphi}_{\text{int}}$  is estimation of spatially correlated parts and  $\Delta\varphi_{\text{DEM}}^{\text{NC}}$

is estimation of non-spatially decorrelated phase of DEM. Pixels with higher value of  $\gamma$  are more likely to be a SFP. Average phase of selected SFP's and also  $\gamma$  are calculated during a repetitive process which leads to noise reduction. It is necessary to choose a threshold value for  $\gamma$ . The Probability density function of whole data is proportion to probability density function of random pixels and SFP's:

$$P(\gamma) = (1 - \alpha)P_r(\gamma) + \alpha P_{SFP}(\gamma). \quad (2)$$

Participation probability of random pixels must be smaller than a certain value:

$$q = \frac{(1 - \alpha) \int_{\gamma_t}^1 P_r(\gamma) d\gamma}{\int_{\gamma_t}^1 P(\gamma) d\gamma}. \quad (3)$$

It is possible to consider no probability for SFP's that the  $\gamma$  for them is less than 0.3. So the value of  $\alpha$  and  $\gamma$  threshold are obtained:

$$\int_0^{0.3} P(\gamma) d\gamma = (1 - \alpha) \int_0^{0.3} P_r(\gamma) d\gamma. \quad (4)$$

In order to detect the wrongly omitted SFP's with high ADI, the process of calculating  $\gamma$  will be done for them (Hooper 2006).

Finally, the unwrapped phase equation reads:

$$\varphi_{uw} = \varphi_{def} + \varphi_{atm} + \Delta\varphi_{orb} + \Delta\varphi_{DEM}^{Corr} + \Delta\varphi_n + 2k\pi, \quad (5)$$

where  $\Delta\varphi_n$  is the spatially decorrelated phase of noise.

### Deformation phase retrieval

The remained phases of recent equation are spatially correlated. However, they consist of both temporally correlated and decorrelated parts. The temporally correlated phases are due to atmospheric noise and orbit errors of master image. So they exist in all interferograms. Since phase  $2k\pi$  has made the phase equation temporally decorrelated, it is impossible to utilize a low pass filter in time domain. With the aim of removing  $2k\pi$  phase, unwrapped differential phase among adjacent pixels is calculated using Delaunay triangulation. Therefore a low pass filter is applicable and temporally correlated phase will be eliminated (Hooper 2006).

A high pass filter could estimate temporally decorrelated phases. The remained noise phase will be omitted by means of a low pass filter in space domain. Lastly the deformation phase will be acquired by estimated phases (Hooper 2006):

$$\varphi_{def} \approx \varphi_{uw} + \widehat{\varphi_{atm}^m} - \widehat{\varphi_{atm}^s} + \widehat{\varphi_{orb}^m} - \widehat{\varphi_{atm}^s} - \Delta\varphi_{DEM}^{Corr} - \Delta\varphi_n - 2k\pi. \quad (6)$$

### 1.2. Finite element modeling

The modeling of materials with linear elastic behavior could be done by means of conventional analytical computing methods. But in case of nonlinear elastoplastic behaviors an advanced numerical approach is desirable which can be solved by a computer software (Gunduz 2008). In this study the PLAXIS software was used (Brinkgreve *et al.* 2006).

There are a wide range of numerical methods of modeling including finite volume, finite element and finite difference. Finite element is an effective way to solve partial differential and integral equations by converting them to ordinary equations. A uniform structure is divided into a number of elements and stress and strain will be calculated in these elements numerically. The elements are connected by nodes which have a degree of freedom. Since stress and strain are available, other parameters like deformation are obtainable simply (Ottosen, Petersson 1992).

The behavior of an element could be defined by a mathematical equation named behavioral model (Gunduz 2008). Depending on materials and loadings, there are lots of behavioral models. Problems with dynamic loadings or creep could be solved by time variant behavioral models. However, in case of static problems with linear elastic, nonlinear elastic and elastoplastic materials, time invariant models are applicable. Embankment dams are massive, anisotropic, heterogeneous and inelastic soil structures which have contact with water and foundation (Segerlind 1984; Dassault Systèmes 2011).

An ideal model should have three main features (Ottosen, Petersson 1992; Dassault Systèmes 2011):

- (1) Material behavior should be simulated as reality under all loading circumstances.
- (2) The model should be simple and based on ordinary mathematical equations.
- (3) The number of required parameters should be as lowest as possible and acquirable by conventional soil experiments.

Due to nonlinear inelasticity behavior of soils, an ideal model is critical. In case of inappropriate models, the results would not be accurate and reliable (Dassault Systèmes 2011).

In this study elastoplastic hardening soil model has been applied. This model is a complicated model which simulates behavior of all kind of soft and hard soils. When initial deflection loading is applied to soil, its hardening will be decreased and irreversible plastic strain will be increased. The relation of axial strain

and deflection stress could be estimated in conditions of drained triaxial experiment. It is possible to use the hardening model instead of hyperbola model by means of plasticity theory instead of elasticity theory, soil dilation angle and defining a yield surface.

### 2. Validation data

Planning and creation of a precise geodetic network around and on a structure is one the most reliable and conventional method to control deformations of that structure. The geodetic network of Masjed Soleiman dam has been planned before dam operation and the field surveying operations have been done in 10 periods so far. The value and direction of network point's deformations on dam from step one to the last step have been depicted in Figure 2.

Also horizontal and vertical displacements of dam along depth are collected by instrumentations to validate modeling results.

### 3. Results and discussion

The image of 2004/12/24 was chosen as master image since the perpendicular and temporal baseline of this image related to another images were small enough. Primary interferograms were created under these conditions: coherence greater than 0.35, perpendicular baseline less than 1070 meter and temporal baseline less than 1500 day. Low quality of interferograms resulted in reduction of SFP's. So the images of low quality interferograms were discarded. Finally, 6 images were processed and 15 interferograms were produced (Fig. 3).

At the end of SBAS process the residuals of all interferograms are less than  $\pi$ . Five main unwrapped interferograms have been plotted in Figure 4. Main interferograms have been produced by master image. Deformations are shown in radian unit. The asterisk is the reference point. Topographic phase has been removed by digital elevation model of Shuttle Radar Topography Mission (SRTM) (Jarvis *et al.* 2008). Flatten earth phase, orbital phase and noise have almost been eliminated.

No significant deformation has been detected between years 2003 and 2004 because dam operation has been done in year 2000 and major changes have happened in first years of operation.

The maximum value of phase difference is observed in image of 26 Sep 2003. Then the image of 5 Dec 2003 has the most phase difference related to master image. One of the reasons is water level changes

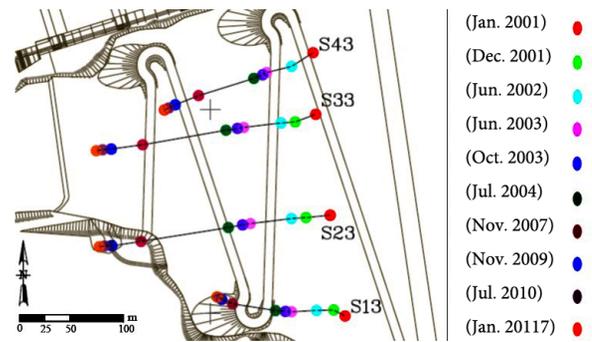


Fig. 2. Direction and value of horizontal displacements of geodetic stations

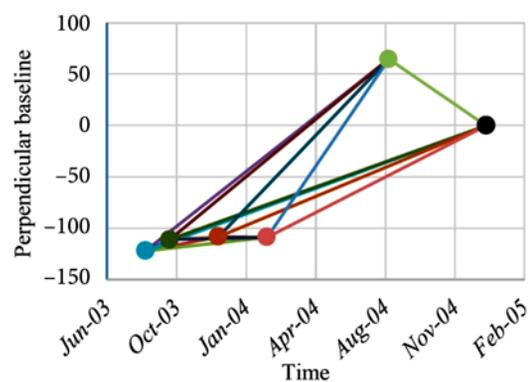


Fig. 3. SBAS network

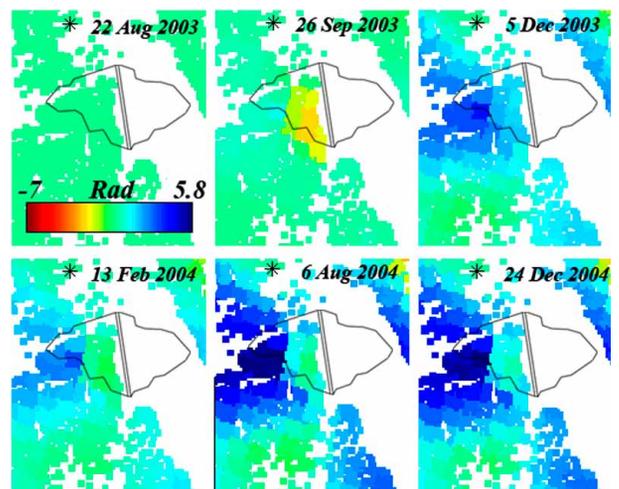


Fig. 4. Main unwrapped interferograms due to master image

between 22 Aug 2003 and 5 Dec 2003 (4.5 meter). The pattern of water level changes in 2004 is similar to what happened in 2003. In summer water level has increased and in winter has decreased. This water level variation has contributed to dam deformation which is depicted as phase differences in interferograms. However, this deformation is too small.

At the end of SBAS processing map of deformation velocities has been retrieved. Figure 5 shows the

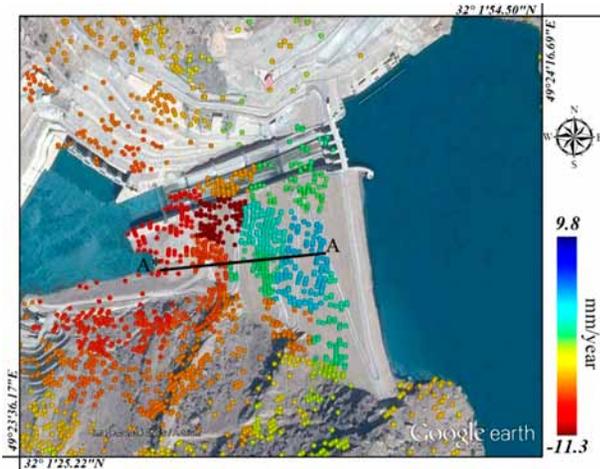


Fig. 5. Velocity map on Google Earth

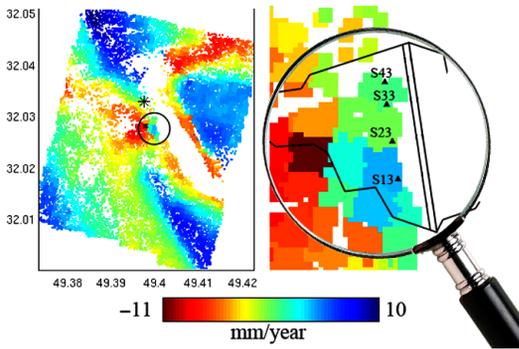


Fig. 6. Location of geodetic stations on velocity map

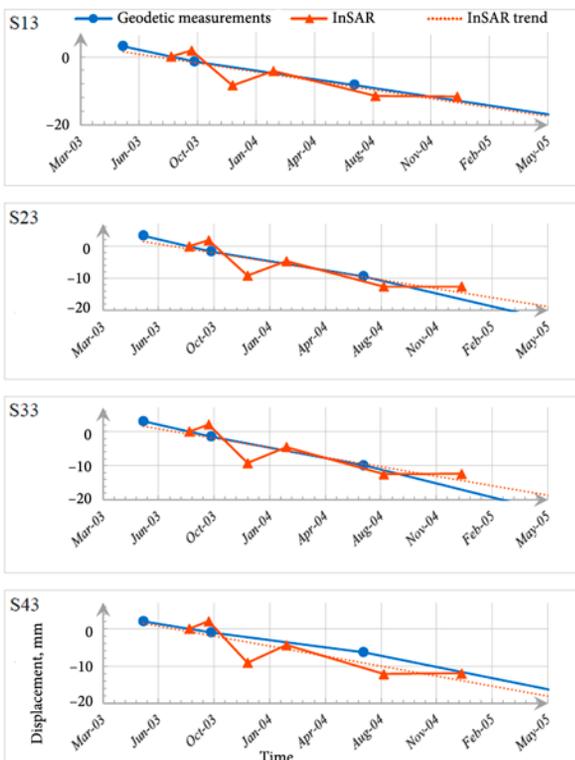


Fig. 7. Comparison of InSAR results and geodetic measurements

velocity map on Google Earth. The middle part of dam moves faster than other parts (3.5 mm/year in direction of Line of Sight). The rate of displacement at lateral sides has declined to 1 mm/year.

Geodetic components of deformation should be transformed to LOS direction to comprise field surveying operation displacements with SBAS results. Eq. (7) is used to transform a three dimensional displacement field to LOS direction (Shamshiri *et al.* 2014):

$$d_{LOS} = -d_x \cos \alpha \sin \theta + d_y \sin \alpha \sin \theta + d_z \cos \theta, \quad (7)$$

where  $d_x$ ,  $d_y$  and  $d_z$  are components of deformation,  $\theta$  is incidence angle and  $\alpha$  is satellite azimuth.

Figure 6 shows the location of comprised points on the dam.

Time interval between first and last image is 490 days. Deformation derived by geodetic measurements has been referred to the reference point of SBAS method spatially and date of master image temporally.

Figure 7 shows the comparison of geodetic measurements and SBAS deformations. Normalized Root Mean Square Errors of points S13, S23, S33 and S43 are 20%, 22%, 23% and 26%. So the average NRMSE is 23%.

### Finite element modeling

Since cross section of 260 meter is the most elevated section, it has been modeled in a plain strain modeling. The main cofferdam with materials of gravel and a temporary crown has been unified with main dam at outer upstream layer. The elevation of dam from lowest part of core trenching is 164 meter. The steepness of upstream is 1 to 2 and downstream steepness is 1 to 1.75. Also the roads are 6 meter wide. Dam crest width is 15 meter. Figure 8 and Figure 9A show longitudinal and 260 cross section of dam.

Hyperbola hardening soil model was used to model dam body and Mohr-coulomb model was utilized for foundation modeling. These models parameters of materials are listed in Table 1 and Table 2.

15-node triangular elements were implemented in modeling. The final mesh had 4725 elements, 38211 nodes, 56700 stress points. Figure 9B has shown meshed dam.

Roller anchor ( $u_x = 0, u_y = free$ ) at lateral sides of foundation and joint anchor at the floor of foundation were applied (Fig. 9B) (Seegerlind 1984). Water level data has been used to produce initial pore water pressure.

There are six calculation phases. Initial stresses were produced at phase one and deformations were

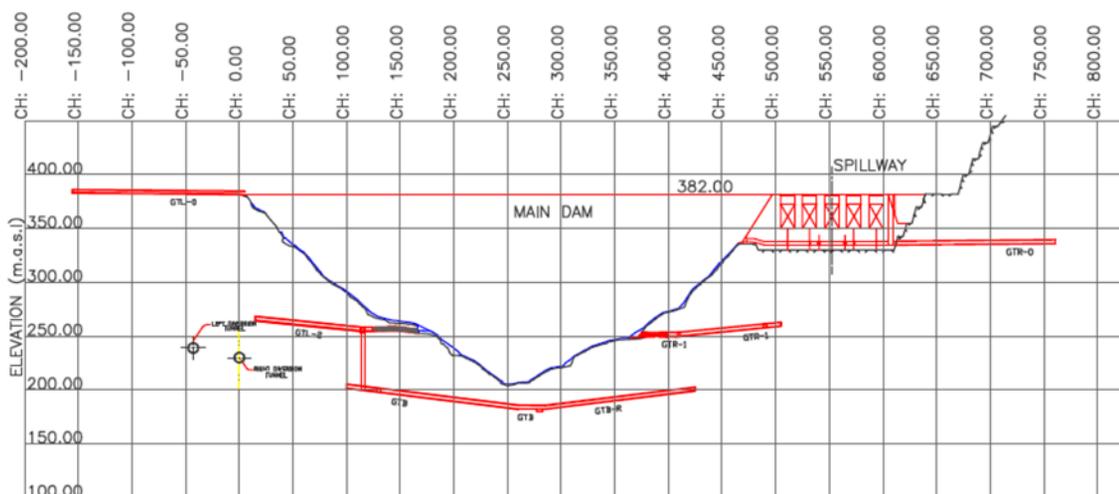


Fig. 8. Longitudinal section of Masjed Soleiman Dam

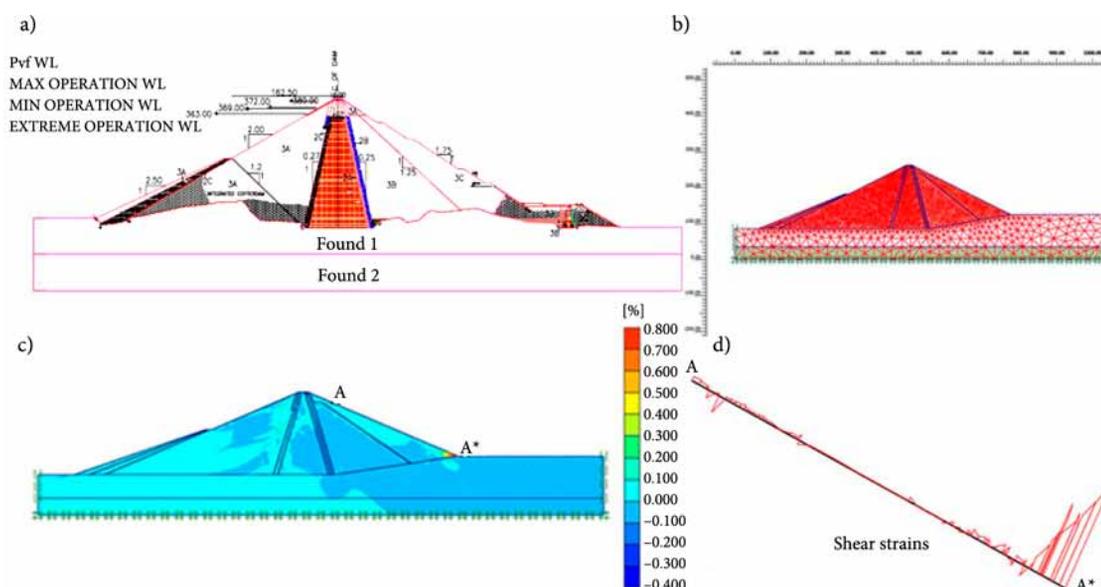


Fig. 9. 260 Cross section of Masjed Soleiman Dam(A), Meshed dam(B), Shear strain (C), Shear strain along line AA\*(D)

Table 1. Material property of dam body in HS model

Material	2A	2B	2C	3A	3B	3C	1 (Core)
Type	Drained	Drained	Drained	Drained	Drained	Drained	UnDrained
$\gamma_{unsat}$ (kN/m <sup>3</sup> )	20.5	18.3	22.9	13.5	22.9	13.5	21.5
$\gamma_{sat}$ (kN/m <sup>3</sup> )	23.2	19.7	23.2	13.5	23.9	13.5	22.5
$K_x$ (m/day)	0.39	0.39	0.009	0.15	0.005	0.15	9e-6
$K_y$ (m/day)	0.32	0.32	0.002	0.18	0.008	0.18	1.3e-6
$E_{50}^{ref}$ (kN/m <sup>2</sup> )	72 000	37 000	126 000	94 000	95 000	94 000	28 000
$E_{oed}^{ref}$ (kN/m <sup>2</sup> )	72 000	56 676	126 000	91 563	95 000	91 563	27 650
$E_{ur}^{ref}$ (kN/m <sup>2</sup> )	216 000	111 000	378 000	282 000	285 000	282 000	84 000
$c^{ref}$ (kN/m <sup>2</sup> )	0	0	0	0	0	0	12
$\phi$ (deg)	35	41	41	45	41.7	45	30.9
$\psi$ (deg)	5	11	11	15	2	15	0
$\nu_{ur}$	0.2	0.2	0.2	0.2	0.2	0.2	0.2
$P_{ref}$ (kN/m <sup>2</sup> )	1200	600	1200	1200	300	1200	600
Power	0.5	0.5	0.5	0.35	0.35	0.35	0.7

Table 2. Material property of dam foundation in Mohr-coulomb model

Material	Found 1	Found 2
Type	Drained	Drained
$\gamma_{unsat}$ (KN/m <sup>3</sup> )	23	24
$\gamma_{sat}$ (KN/m <sup>3</sup> )	24	25
$K_x$ (m/day)	0.0086	0.8640
$K_y$ (m/day)	0.0086	0.8640
$\nu$	0.3	0.3
$E_{ref}$ (KN/m <sup>2</sup> )	38 772 200	6 776 400
$c_{ref}$ (KN/m <sup>2</sup> )	700	2000
$\varphi$ (deg)	30	45
$\psi$ (deg)	0	12

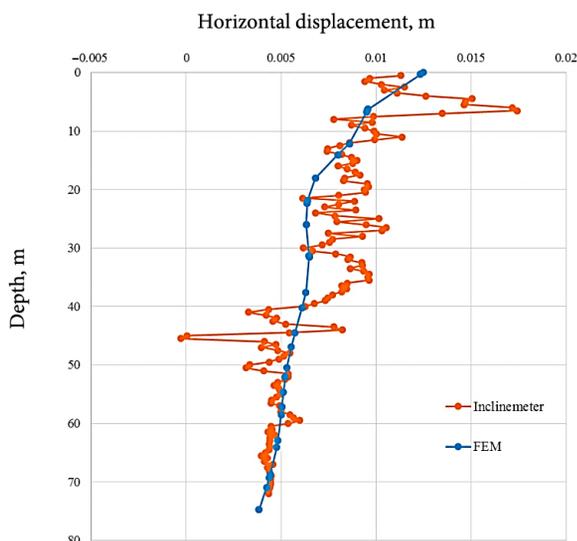


Fig. 10. Evaluation of horizontal displacements of modeling and instrumentations versus depth

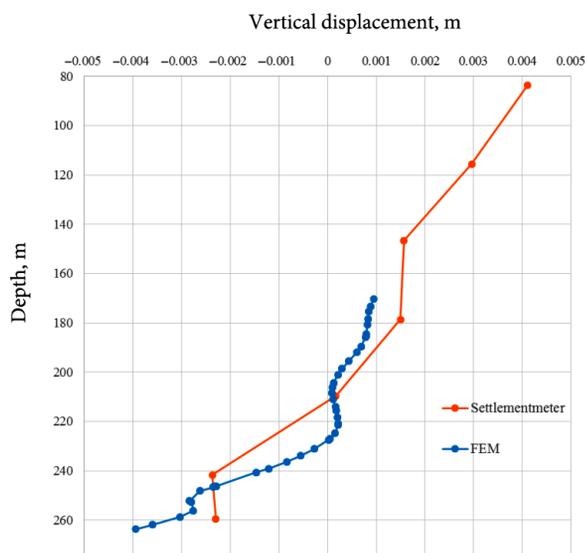


Fig. 11. Evaluation of vertical displacements of modeling and instrumentations versus depth

calculated at the other phases. According to time difference between first image and last image, the time interval of modeling is 490 days. Deformation derived from SBAS has been imported as an initial condition in modeling.

Figure 9C illustrates shear strain at the end of processing. Also shear strain in AA\* direction was plotted in Figure 9D.

This is observed that shear strain has reached to a maximum value at the lowest elevation of downstream. AA\* line has been drawn on the velocity map in Figure 5. High deformation gradients in the lowest elevation of downstream have a good consistency with modeling results.

In order to validate modeling results the instrumentations data of dam were obtained. Inclinometer and settlement meter measure horizontal and vertical movements. These measurements versus depth are plotted along with modeling results. Figure 10 and Figure 11 shows the evaluation.

### Conclusions

The purpose of this study is to examine the displacements of embankment dams. The time history of embankment deformations has been retrieved using Interferometric SAR. Subsequently the deformations derived from InSAR have been used as an initial condition in Finite Element Modeling. Due to valuable features including non-contact measurements, all weather compatibility and high spatial resolution, InSAR is a powerful tool to obtain surface movements with an acceptable accuracy. Moreover, it is possible to be aware of dam behavior in future and investigate the source of its displacements using FEM. At first 19 ASAR images of ENVISAT sensor with 56 mm wavelength and incidence angle of 23 degrees was processed. Lastly 6 images between years 2003 and 2004 were selected for final processing. The validation has been done for four points on the dam body by precise field surveying operations. The comparison shows a good agreement between Interferometry results and geodetic measurements. The retrieved NRMSE is between 20% and 26%. Furthermore, calculated horizontal and vertical displacements in modeling were compared with instrumentations data. The results approve that modeling has a good consistency with instrumentations.

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